



Recent investigations of TS-MME for the CLIC project

## Characterisation of the METSO CuZr/Mo prototype rod obtained by HIP diffusion bonding

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  - c. Soundness of the interface
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## Aimed structure







## The Mo + 99.85Cu-0.15Zr system : 1) C15000 alloy



Typical heat treatment:

- ♦ Solution annealing  $\Rightarrow$  Nominal T, t = 900 to 925 °C,
- 5 to 30 min, fast cooling
- ♦ (In reality HIP quenching from 900 °C, 10 h (!), cooling 20 °C/min)
- ♦ Artificial aging (aged only)  $\Rightarrow$  T, t = 550 °C, 3 h



## The Mo + 99.85Cu-0.15Zr system :



## Table 18 Typical mechanical properties of C15000

Section size		Cold work, %, after:		Tensile		Yield		Florestion(b)
		Solution		strength		strengtn(a)		Liongation(D),
mm	in.	treating(c)	Aging(d)	MPa	KSI	MPa	KSI	70
Rod	•			ν.				
5	0.20	• • •	76	430	62	385	56	8
6	0.25	10(e)	• • •	285	41	250	36	34
9.5	0.37	80	44	470	68	440	64	11
13	0.50	56	47	460	67	435	63	15
16	0.62	61	31	440	64	430	62	15
19	0.75	.50	34	435	63	420	61	15
22	0.87	48	52	430	62	415	60	15
25	1.0	48	47	430	62	415	60	15
32	1.25	32	17	430	60	400	58	18
Wire								
1	(0.04)	• • •	<b>98(f)</b>	525	76	495	<b>72</b>	1.5
2.3	(0.09)		<b>62(f)</b>	495	72	470	68	3
		0		200	29	40	6	54
1.1			0	205	30	90	13	49
6	(0.25)	0(e)(g)	• • •	255	37	75	11	50
13	(0.50)	30(e)	•••	365	53	340	49	23

a) At 0.5% extension under load. (b) In 50 mm or 2 in. (c) At 900 to  $925 \,^{\circ}C$  (1650 to  $1695 \,^{\circ}F$ ). (d) For 1 h or nore at 400 to  $425 \,^{\circ}C$  (750 to  $795 \,^{\circ}F$ ). (e) Mill annealed. (f) Solution treated, cold worked the stated mount, then aged. (g) OS025 temper.



Strength of zirconium-copper depends primarily on cold working. Aging results in some increase in strength, and an increase in electrical conductivity



	Solution-	Amount of cold work,	Agir	ng			Elongation,	Hardness, HRB	Electrical conductivity, % IACS	
	treating temperature	%	Tempe- rature	Time, h	Tensile strength	Yield strength	70			
	<b>3</b> °		<b>3</b> °		MPa	MPa				
	900	20	475	1	310	260	25	48	85 min	
rh	900	80	425		425	380	12	04	<del>85 min</del>	
	980	None			200	41	54		64	ī
	980	20			270	250	26	37	64	
	980	80			440	420	19	73	64	
	980	None	500	3	205	90	51		87	
	980	None	550	3	205	90	49		95	
	980	20	400	3	330	260	31	50	80	
	980	20	450	3	330	275	28	57	92	
	980	85	400	3	495	440	24	79	85	
	980	85	450	3	470	425	23	74	91	





## Diffusion bonding by HIP (courtesy of Metso)



#### Part Manufacture

The joint surface of completed shape of the part and the work method for the capsule assembly are examined, and part manufacture is executed under consideration of the shape of each part and the finishing allowance.

#### Capsule Assembly

Dirt, oxide layers, etc., are removed completely from all parts, and then all the connection parts are sealed by welding with capeule material with good weldability to prevent oxidation.

## Vacuum Sealing

The capsule is checked for leakage, and then the inside is evacuated for vacuum sealing. At this time, heating is done during the evacuation in order to obtain a higher vacuum. This step is not required when capsule assembly is done by EB welding.





# Bimetallic structures







## Microoptical observations, CuZr matrix and Mo insert



grain size across the bimetal section







Microoptical observations, CuZr matrix and Mo insert



## □As-received state (HIP-quenched):

- Cu-Zr matrix: grain size, approximately 70  $\mu$ m
- Increasing from centre to periphery?
- · Mo insert: cross-sectional grain size, approximately 25  $\mu$ m
- Presence of an envelope adhering poorly to the Cu-Zr matrix



## Mechanical properties, hardness and microhardness profiles







HIP-quenched Cu-Zr, compares to fine grained, annealed Cu-OFE

Mo is not significantly softened by the HIP-cycle. Light softening occurs progressively with time at T

Sample	Rp0.2 /MPa	Rp0.5 /MPa	Rm /MPa	A /%	toct
HIP-quenched Metso	64	73	216	55	S S S S S S S S S S S S S S S S S S S
OFE/OFCu, OS050	-	69	220	45	temper
C15000, 6 mm wire, mill annealed OS025	-	75	255	50	
HIP-quenched CERN	79	90	212	40	
Aged 550°C, 3h Metso	60	70	214	57	
7.2				8.00	







Hall-Petch relationship for copper with grain sizes of 1 mm–3  $\mu$ m (Kozlov, 2002):

 $\sigma = \sigma_0 + k \cdot d^{-1/2}, \ k = 0.14 \pm 0.05 \text{ MPa} \cdot \text{m}^{1/2}$ 

Δσ (25 μm .. 70 μm) ~ 7 MPa .. 15 MPa

FIG. 201. — Variation de la limite d'élasticité conventionnelle du cuivre (pour des déformations de 0,001 et 0,5 p. 100 en fonction de la dimension des grains (d=diamètre en microns).



Mechanical properties, tensile properties of the CuZr matrix



□ As-received state (HIP-quenched):

- Metso and CERN results are consistent
- The HIP-quenched state is not susceptible to directly harden following on ageing treatment

Alliage		Etat		Résistance	Limite	Allonge	Cond.	
				traction	élastique	ment	électrique	
				[MPa]	[MPa]	[%]	[%IACS]	
	C15000	OS025	(recuit, grain < 25 µm)	255	75	50		
		<b>TB00</b>	(mis en estution)	200	41	54	64	Ь
		TF00	(TB00+vieilii)	205	- 90	50	87 - 95	Þ
		TH02	(TB00+écroui ½dur+vieilli)	358	316	15		1
		TH04	(TB00+écroui dur+vieilli)	470	425	23	91	
	Cu-OFE	OS025	(recuit, grain < 25 μm)	235	79	55	100	
		OS050	(recuit, grain < 50 μm)	220	69	55	100	





# Scaning Ele







# Strength and characterization of the interface



A typical diffusion length:  $x^2 = D(T)$ -t where  $D(T) = D_0 exp(-Q/RT)$ 

and D(T) is the interdiffusion coefficient at the temperature T, Q is the activation energy and R is the universal gas constant

Cu7r

10µm (long. scale)

).5um

Q = 146 kJ mol<sup>-1</sup> D<sub>0</sub> = 2.82 10<sup>-10</sup> m<sup>2</sup> s<sup>-1</sup>

x = 1.78 µm, in agreement with the measured profile





# X-Ray diffraction







## Strength and characterization of the interface





Shear surface as from a SEM observation and distribution map of Cu (red), Mo (blue) et Zr (green)



# Strength and characterization of the interface



# Topographical aspect of the sheared interface





Sheared-off interface

## d characterisation face, tensile tests





Estimated (bulk as HIP-quenched CuZr): Rp0.2 = 85.3 (79) MPa Rm = 233 (212) MPa

## Strength and characterization of the interface



## CuZr-Mo interface

- Despite the presence of an intermetallic phase Mo<sub>2</sub>Zr...
- The shear strength of the bimetal interface is higher than the one of the CuZr matrix
- Interdiffusion has occurred as foreseen from diffusion parameters of the Mo-Cu system
- Locally cavities are observed (not expected following a HIP process)
- EDM resulted in one case in a separation of the two phases



## Evolution of HIP-quenched CuZr with further thermal treatments



## **Profile of microhardness for different thermal treatments**





## Evolution of HIP-quenched CuZr with further thermal treatments



## Mo

 No influence on hardness of an additional solution annealing and of further low temperature ageing treatments

## □*C*uZr

- HIP-quenched and solution annealed states are comparable in hardness
- Artificial ageing (550 °C, 3h) is effective after further solution annealing
- Hardness increases from less than 50 HV (annealed states) to approximately 65 HV (solution annealed + aged state)
- For the aged state, increase of microhardness from centre to periphery (Zr depletion)?





- 1. HIP quenching results in a temper state that requires further solution annealing to be susceptible to age
- 2. Ageing after further solution annealing is effective (more or less depending on the position?)
- 3. Depletion of Zr due to diffusion toward the insert-matrix boundary?
- 4. The interface shows (locally?) good interdiffusion and high shear strength
- 5. EDM resulted in a separation of the matrix and the insert (due to the process or to locally poor adhesion?)
- 6. Presence of a Cu envelope?