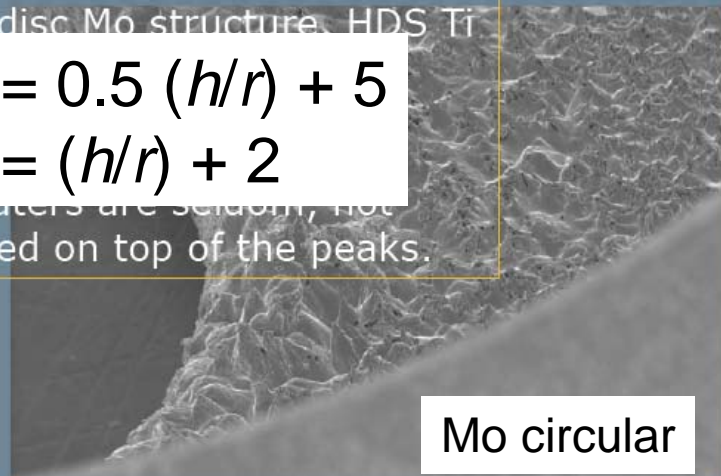


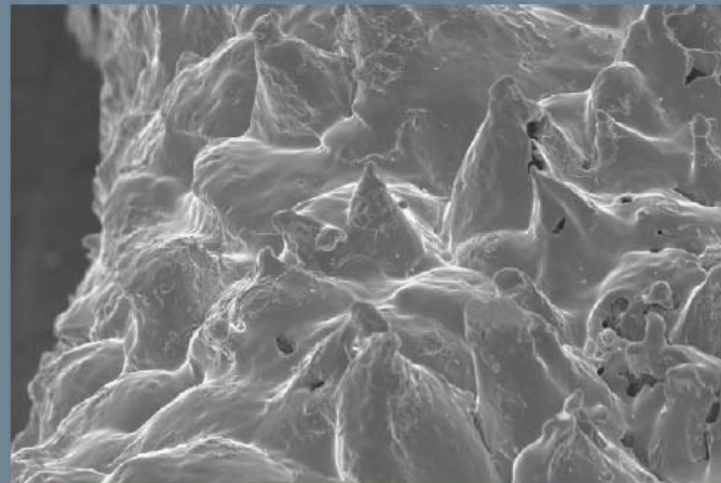
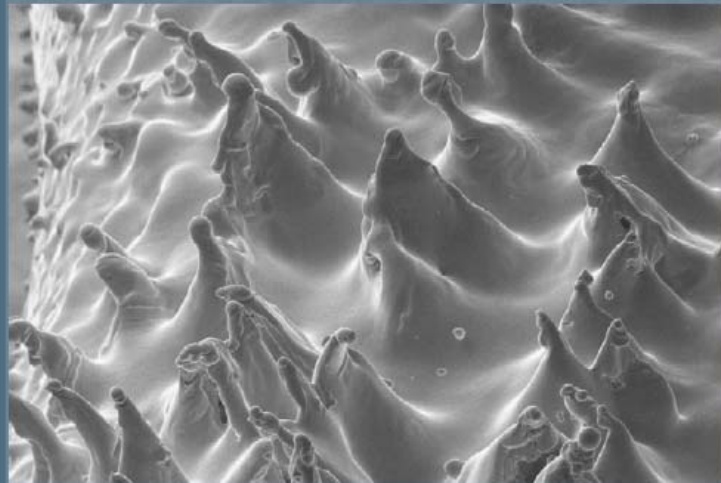
# A few considerations on breakdown phenomena

- Some “anecdotes”
  - Beta values from SEM
  - Taylor cones
- Temperature rise calculations
  - 1D, 2D, 3D heating
  - Heating of tips by field emission currents
- (Nervous...) breakdown rate

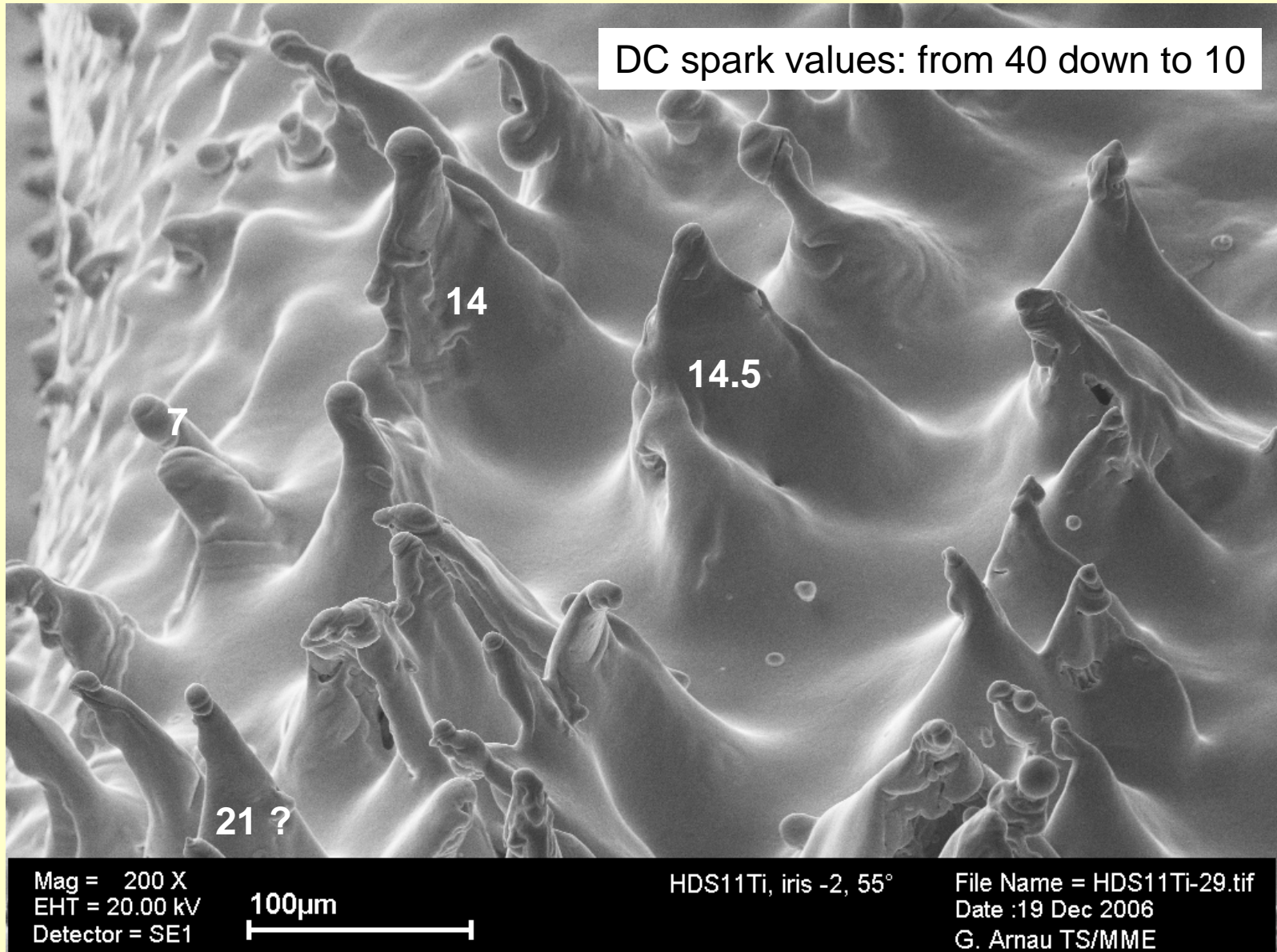
# Comparison of cones in HDS11 Ti and Mo disc structure.



Compared to disc Mo structure, HDS Ti  
*Cone:*  $\beta = 0.5 (h/r) + 5$   
*Cylinder:*  $\beta = (h/r) + 2$   
clusters of craters are seldom, not always localized on top of the peaks.

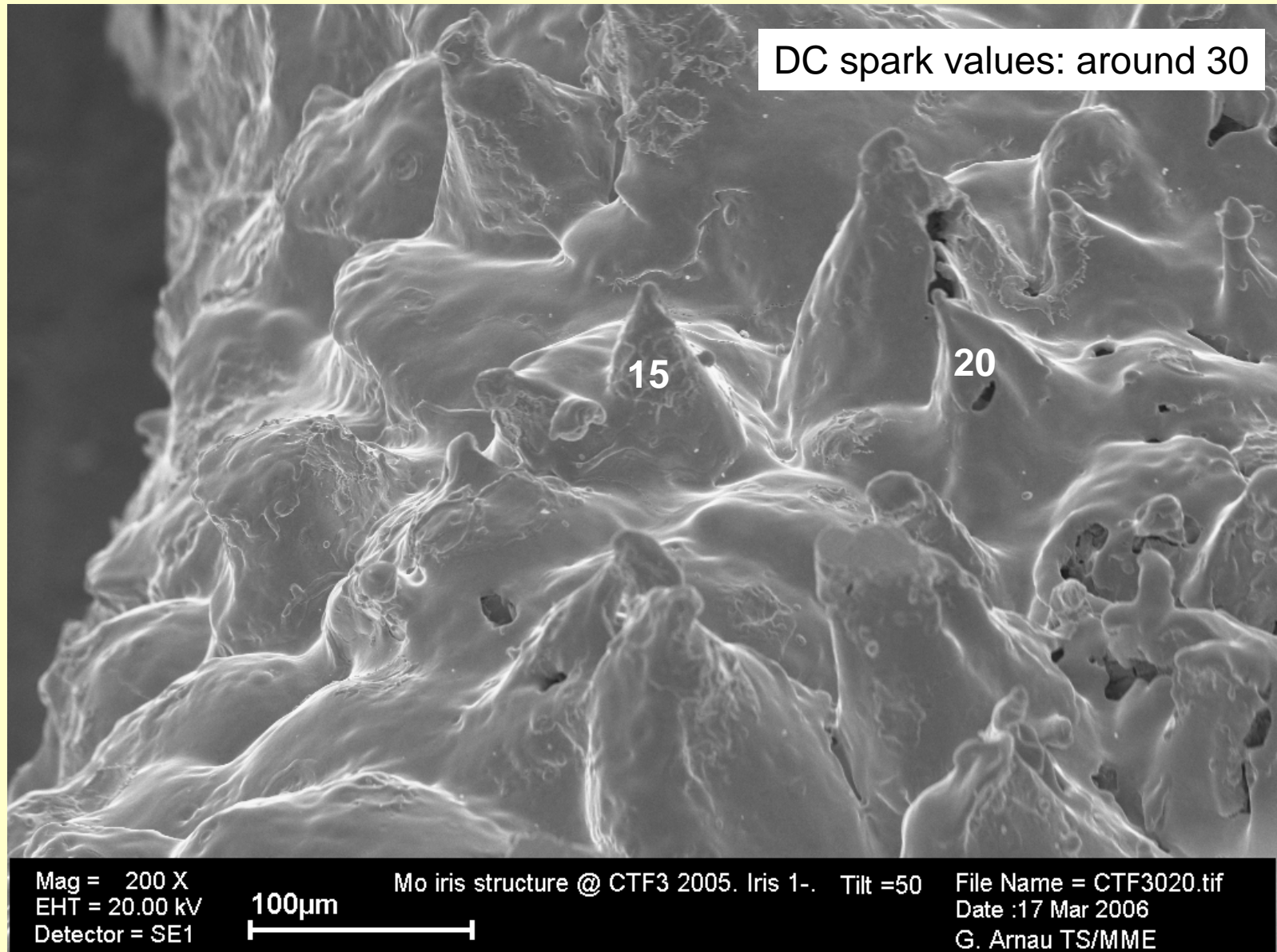


# Beta calculations from SEM observation - Ti





# Beta calculations from SEM observation - Mo



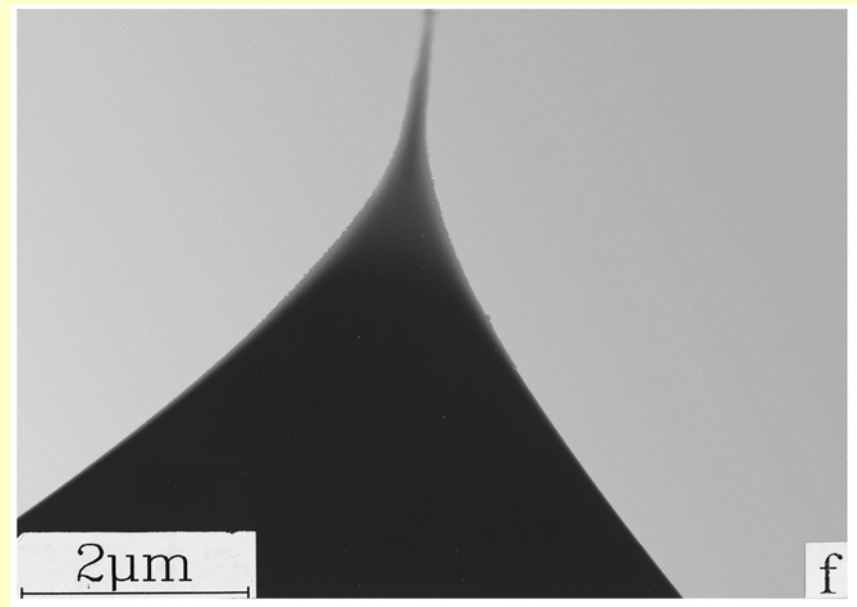
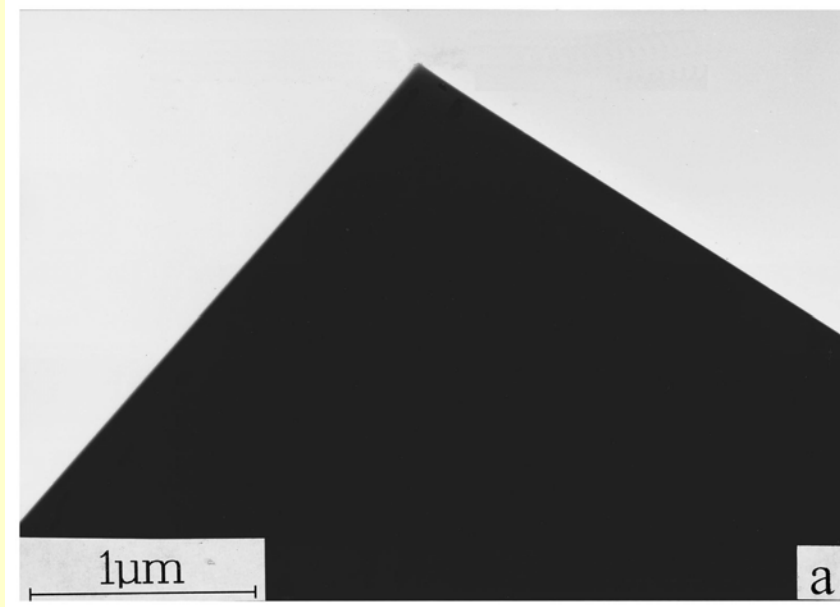
# Pulling of liquid? Taylor cones

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- The “cones” might be the result of the E field pulling over the molten metal. Models of this process exist in the literature.
- When a molten metal is pulled with an electric field, the metal surface is deformed. The resulting shape is due to the balance between the electrostatic force and the surface tension.
- At the highest field the limiting shape is conical, with an half-opening angle of 49.3 degrees (Taylor cone, Proc. Roy Soc. A 280 (1964) 383).
- This shape is independent of the material. When further increasing the field, ion emission starts with a jet. Locally, the atoms binding energy is overcome by electrostatic forces.
- The shape and dynamics of the jet depend on viscous forces
- This process is used in so-called Liquid Metal Ion Sources (for example Cs)

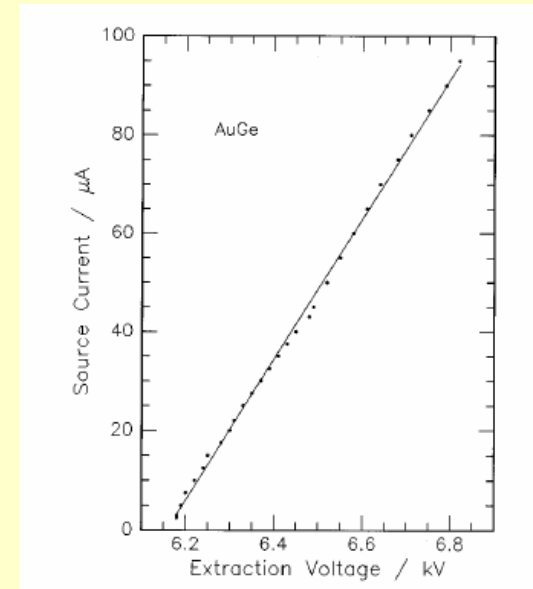


# Taylor cones - images



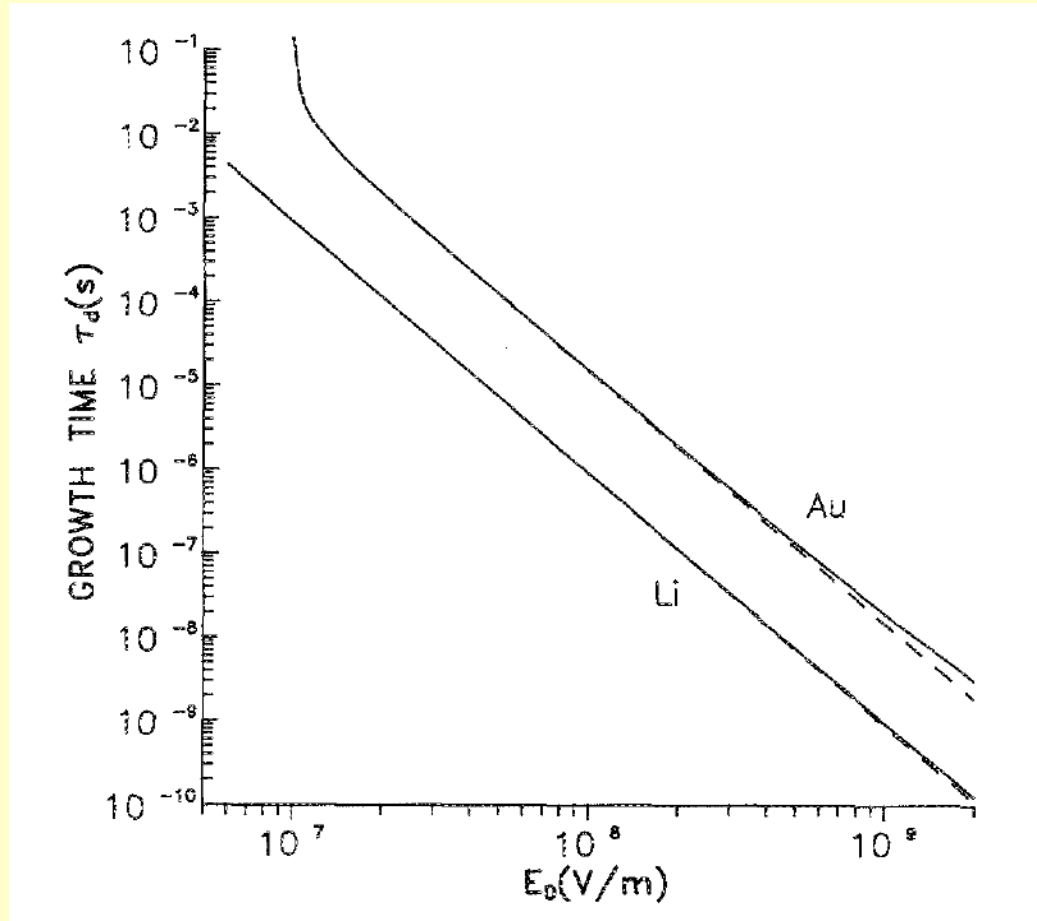
(From Driesel et al. J. Vac. Sci. Technol. B 14 (1996) 3367) - AuGe alloy

- Shape with minimal ion emission (angle close to theoretical value) – left
- Shape with strong ion jet emission - right. Ion current 95 μA, Field 6.8 kV / 1.5 mm, estimated jet diameter 175 nm.
- ⇒ flux =  $6 \cdot 10^{14}$  ions/sec
- ⇒ equivalent pressure = 2.5 bar



# Taylor cones: time for formation I

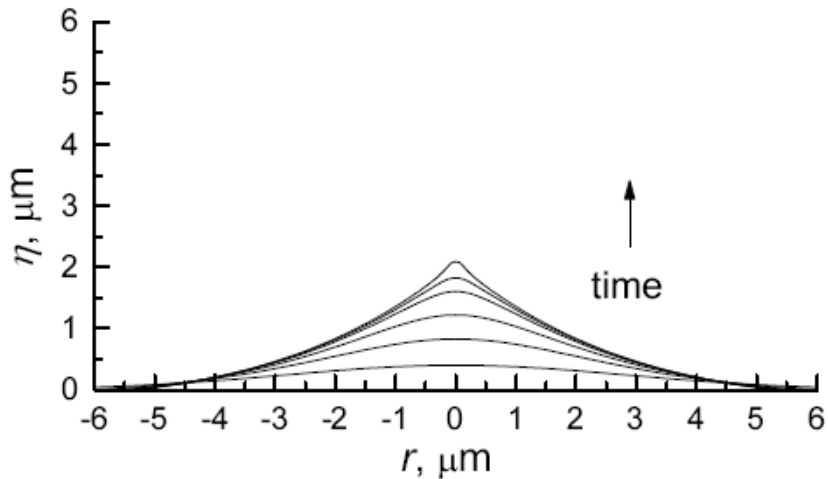
- Formation of instability waves on a flat molten surface (He et al. J. Appl. Phys. 68 (1990) 1475)



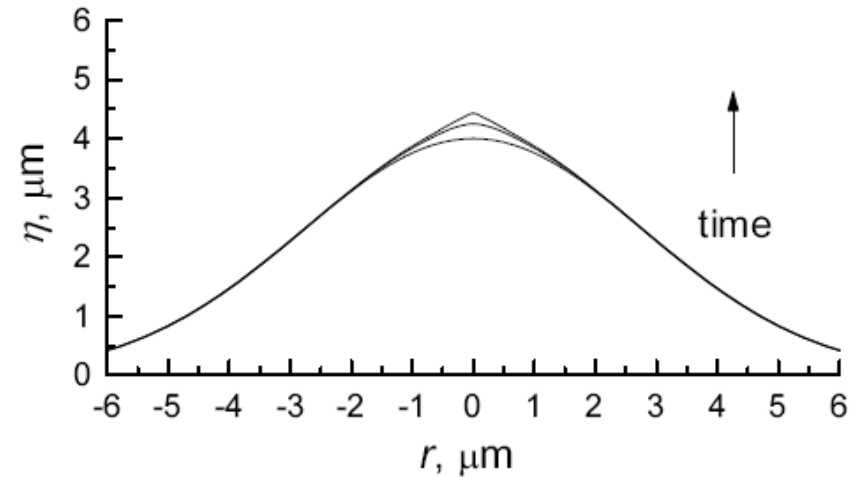
- Seems slow compared to CLIC situation

## Taylor cones: time for formation II

- Growth time of cones (Suvarov et al. J. Appl. Phys. D 33 (2000) 1245) – Mercury at 240 MV/m applied field



**Figure 2.** The surface time evolution; initial form is Gaussian with  $\lambda = 4 \mu\text{m}$ ,  $h = \lambda/10$ . The surfaces are consecutively represented at time: 0, 0.56, 0.73, 0.81, 0.83 and 0.85  $\mu\text{s}$ .



**Figure 3.** The surface time evolution; initial form is Gaussian with  $\lambda = 4 \mu\text{m}$ ,  $h = \lambda$ . The surfaces are consecutively represented at time: 0, 0.048 and 0.057  $\mu\text{s}$ .

- Growth time can be very fast depending on starting conditions



# Temperature rise calculations

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- Here starts the main part of the talk
- 1D, 2D, 3D time dependent heating
  - Relevant for the discussion on breakdown limit
- Heating of tips by field emission currents
  - Relevant for the discussion on breakdown probability

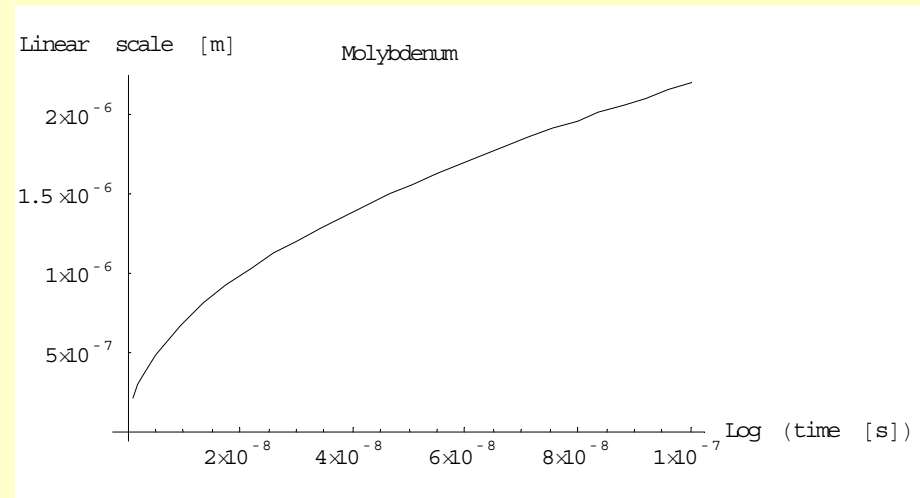
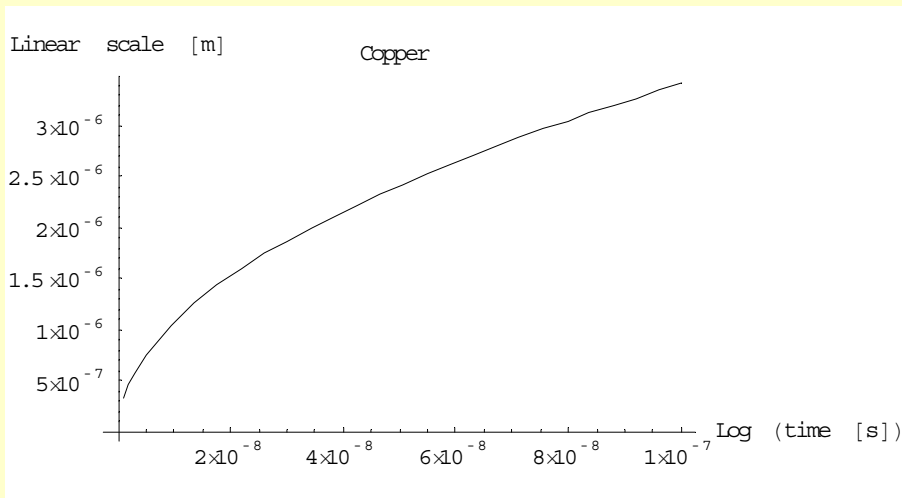


# Time-dependent heating

- The breakdown limit of materials in RF tests is observed to follow the dependence:  $P\tau^a$  with  $a=1/3$  for copper and  $a=2/3$  for molybdenum
- Is there any intrinsic material dependence? Heat flow equation:

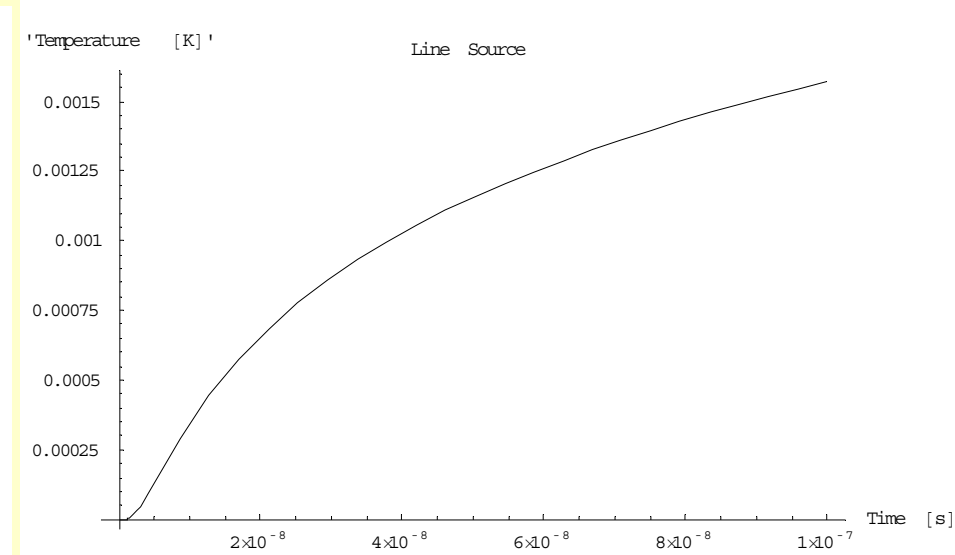
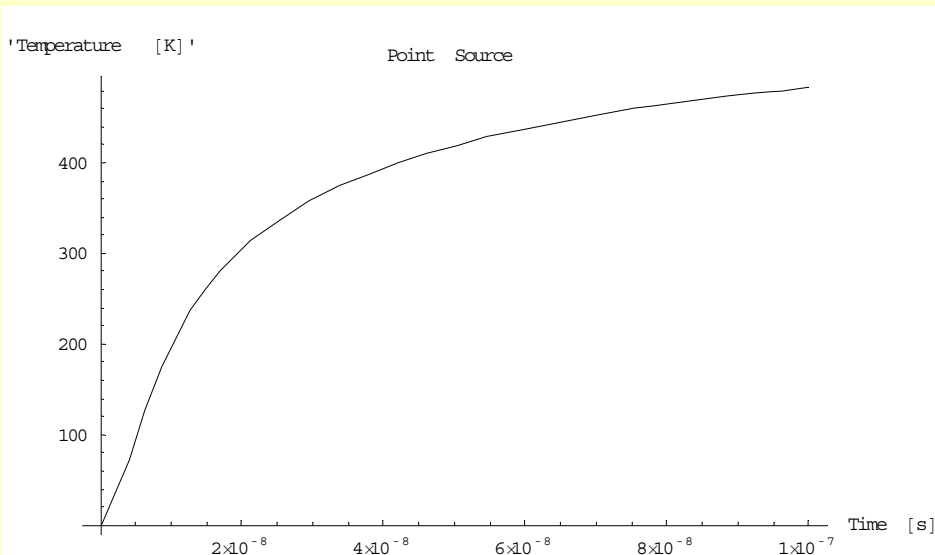
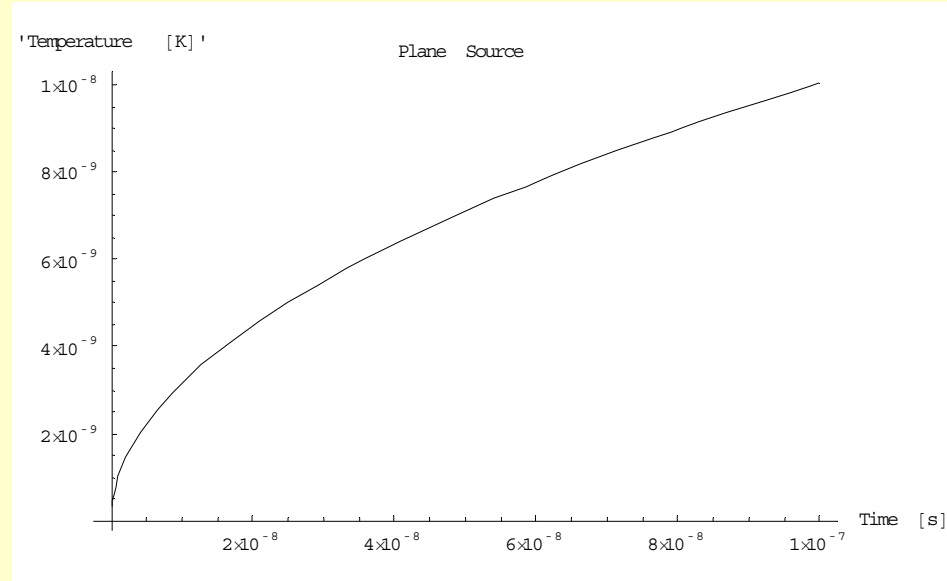
$$\nabla^2 T + \frac{\dot{q}}{k} = \frac{1}{\alpha} \frac{\partial T}{\partial t}$$

- With:  $k$  = thermal conductivity,  $\alpha = k/(c*\rho)$ ,  $c$  = specific heat,  $\rho$  = density
- In-time dependent calculations the distinction between a “fast” and “slow” regime is based on the diffusivity time  $\tau_D = R^2/\alpha$ .  $R$  is the linear scale of the phenomena that are under consideration

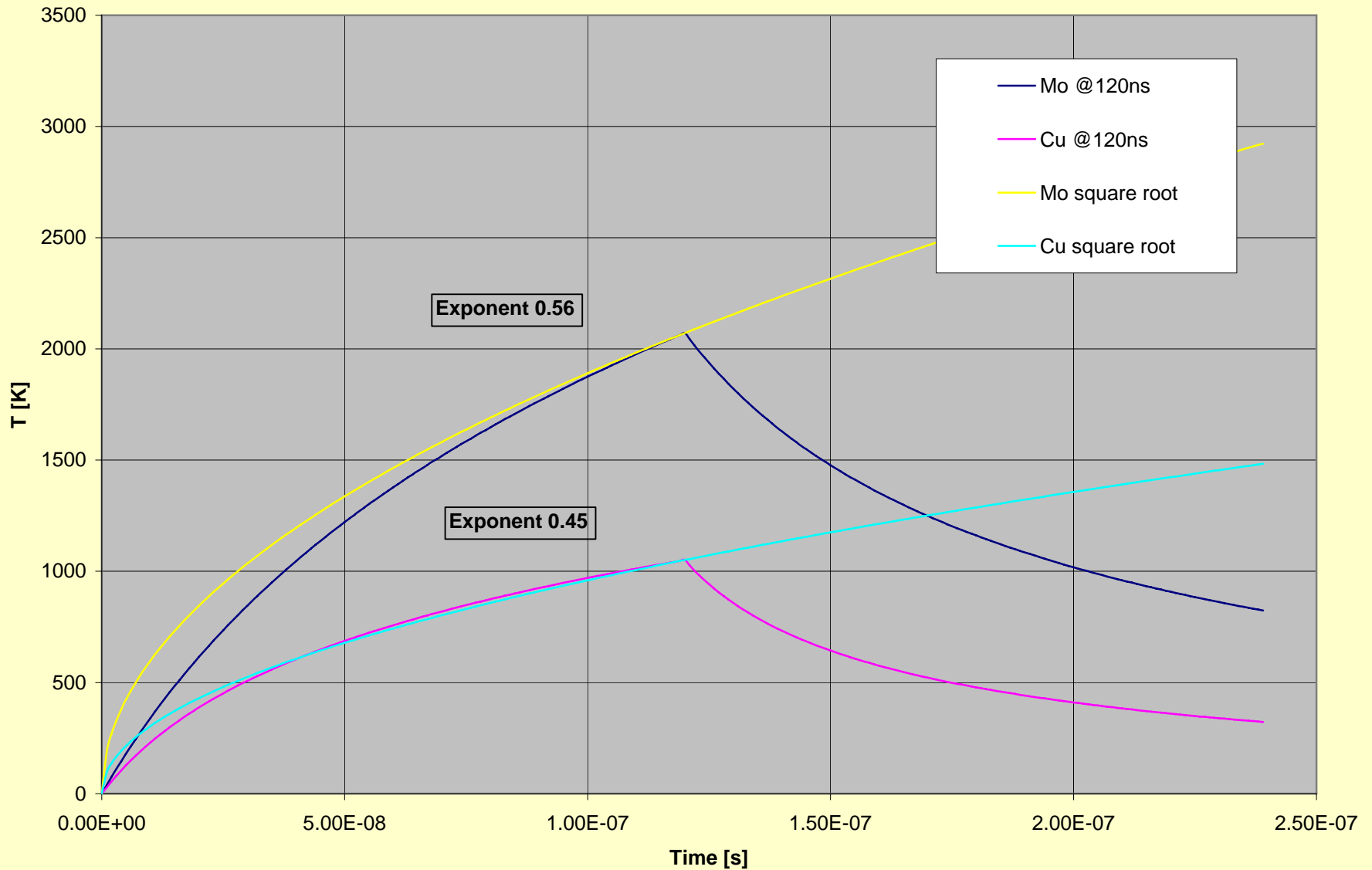


# 1D, 2D, 3D heating profiles inside a solid, or over a semi-infinite solid

- Clockwise:
- 1D heat flow → plane source gives square-root time dependence
- 2D heat flow → line source
- 3D heat flow → point source



# From Alessandro Bertarelli: $2\mu\text{m} \times 2\mu\text{m}$ heat source

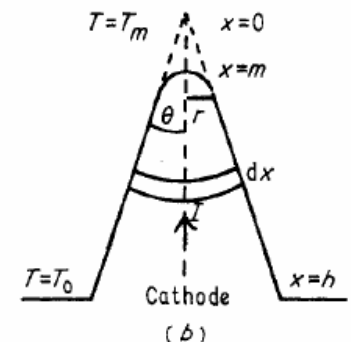
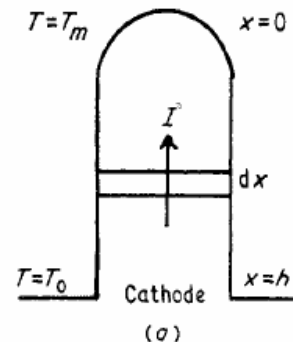


# Heating by field emission

- Field emission currents heat a (conical) tip by Joule effect. The tip is assumed to have a fixed temperature at its base and have a temperature gradient along its height.
- If the resistivity is considered temperature-independent, a stable temperature is achieved (Chatterton Proc. Roy. Soc. 88 (1966) 231)
- If the resistivity (and the other material parameters to a lesser extent) is temperature dependent, then when it increases there is a larger power dissipation, resulting in a further increase in temperature and so on (Williams & Williams J. Appl. Phys. D 5 (1972) 280).
- Below a certain current threshold, a stable regime is reached
- Above the threshold, a runaway regime is demonstrated

- The  $T(t)$  can be calculated.

$$\frac{\partial T}{\partial t} = \frac{K}{\sigma S} \left( \frac{\partial^2 T}{\partial x^2} + \frac{2}{x} \frac{\partial T}{\partial x} \right) + \frac{\rho}{\sigma S} \left( \frac{I}{2\pi x^2(1 - \cos \theta)} \right)^2.$$

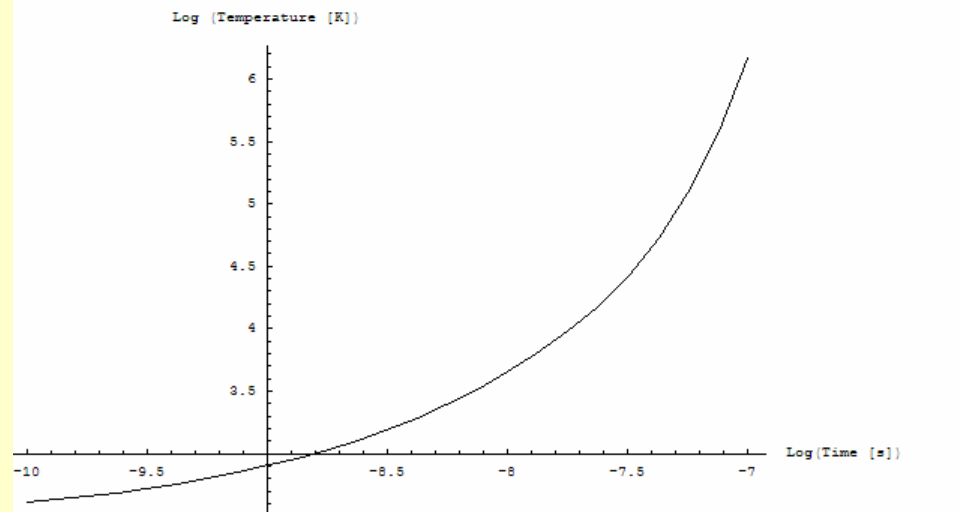
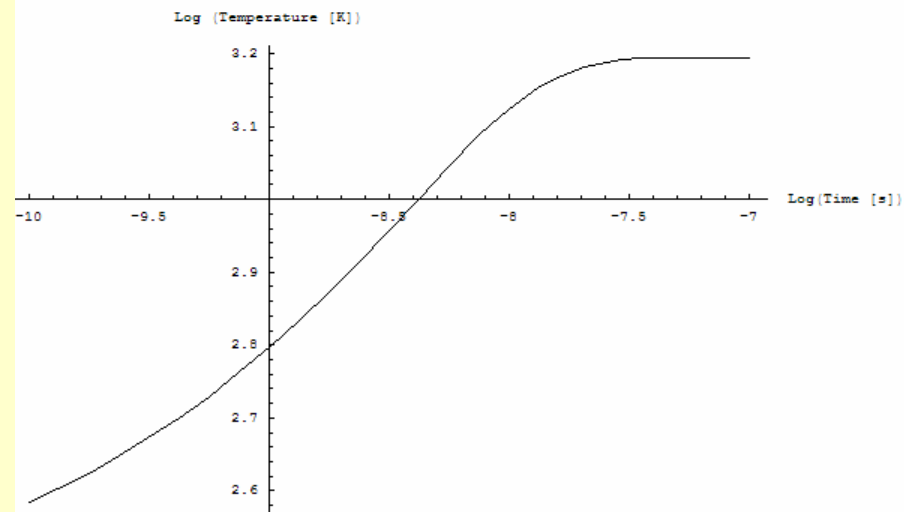
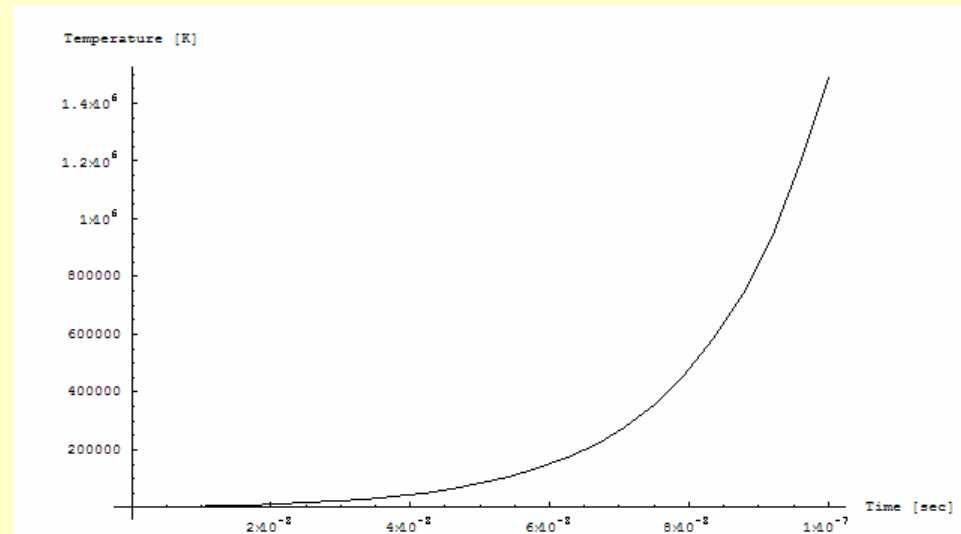
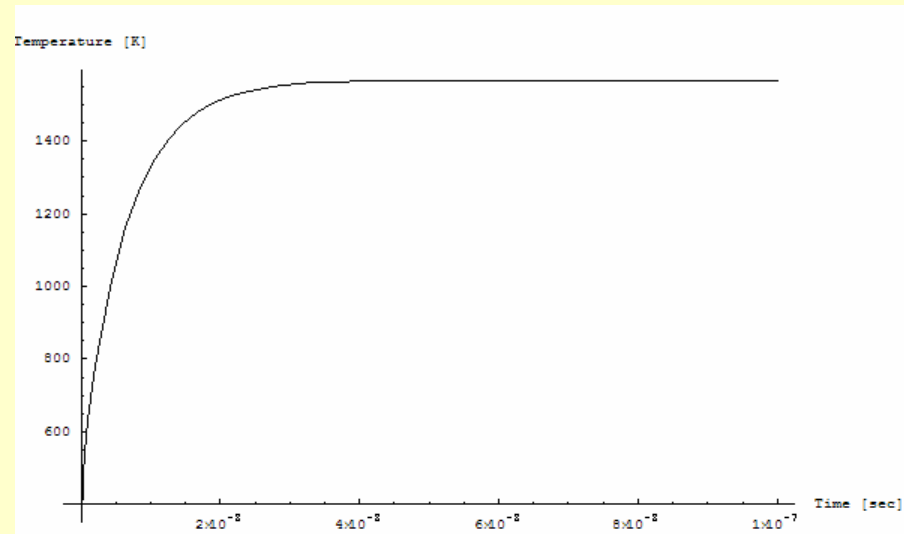




# Simulation for Mo cone: diameter 20 nm, beta = 30

**E=374 MV/m**

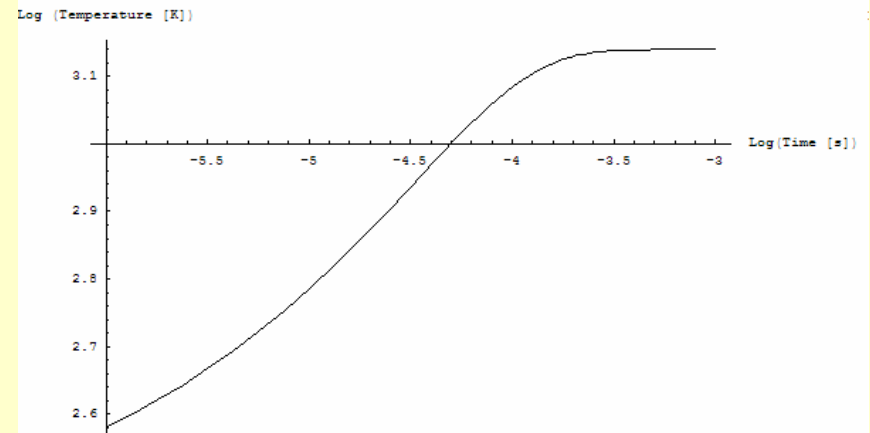
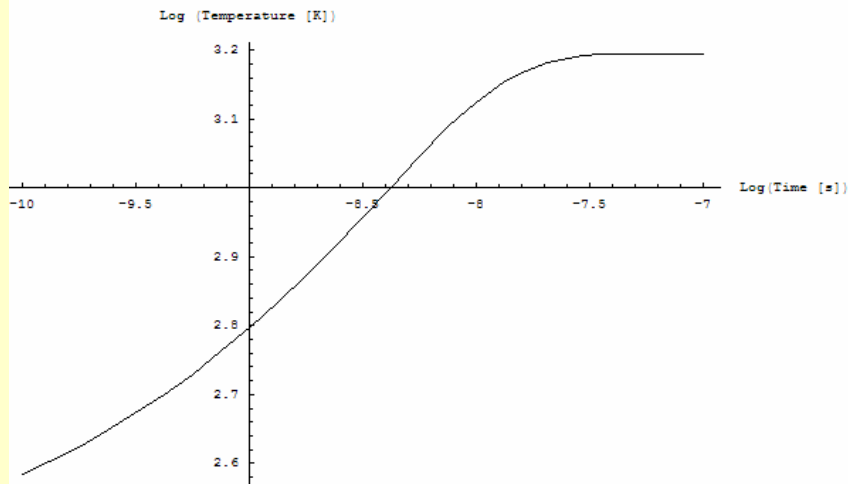
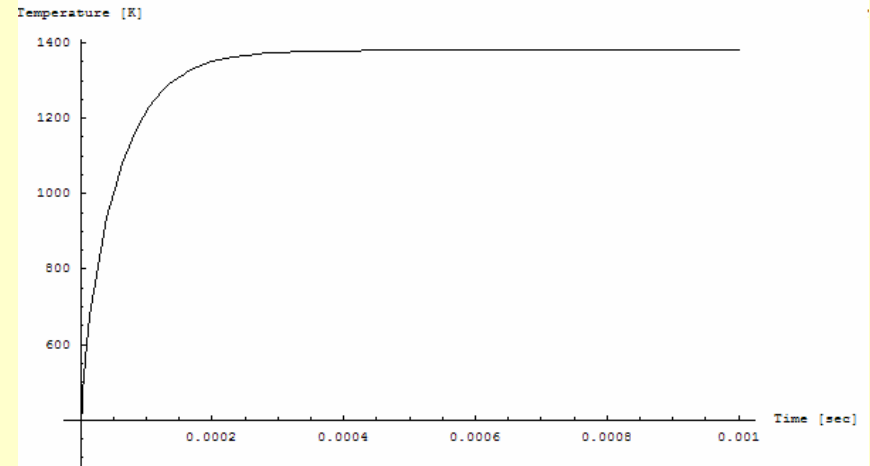
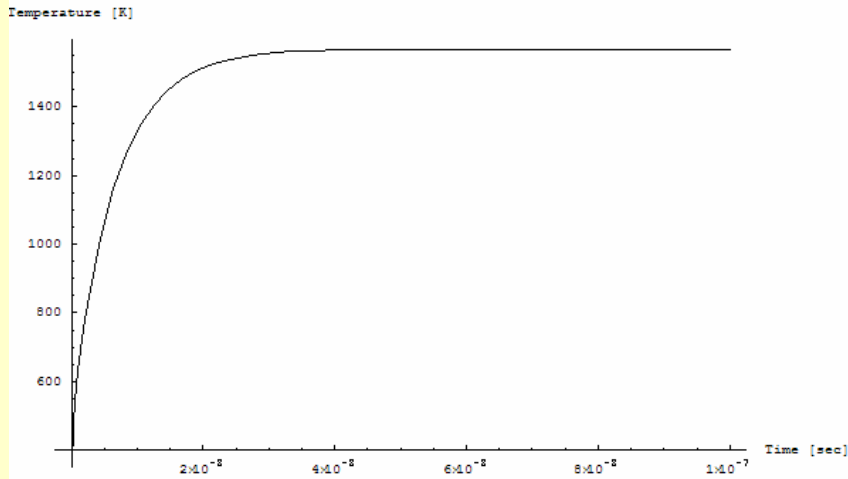
**E=378 MV/m**



# Simulation for Mo cone: beta = 30

**Diameter 20 nm, E=374 MV/m,  
current = 0.028 A**

**Diameter 2000 nm, E=226 MV/m,  
current = 2.8 A**



# Heating by field emission II

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- The current threshold for runaway depends on the diameter of the cone
- The time constant appears to depend on the (diameter)<sup>2</sup> of the cone
- The final temperature (if stable) depends on (thermal conductivity)<sup>-2</sup>
- The rate of temperature increase is (time)<sup>0.5</sup> below runaway
- The rate of temperature increase depends on (thermal conductivity)<sup>-0.5</sup> (???)
- The dependences on the electrical conductivity are the same as for the thermal conductivity



# Thoughts on breakdown rate

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- Is it possible to model the breakdown rate probability starting from simple phenomena?



## Comparison with breakdown rate measurements?

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- The breakdown probability:  $P(x_1, x_2, \dots, x_n) = f(x_1)f(x_2)\dots f(x_n)$
- Where  $x_i$  might be  $E$ ,  $\tau$  or a even a combination of these or other physical quantities.
- I make the assumption that the ignition of a breakdown is due only to gas ionisation by electrons. A breakdown is of course an ionisation cascade
- I assume that the probability of igniting a cascade depends linearly on the amount of gas available and on the primary electron current
- In this case:

$$P_{breakdown} \propto I_{electrons} pressure_{gas}$$

- Normalisation should of course be applied
- Where do the electrons and the gas come from?





## Comparison with breakdown rate measurements?

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- The electron current is given by the standard Fowler-Nordheim equation:

$$I_{electrons} = FN(\beta E)$$

$$FN(\beta E) = Const * (\beta E)^2 \exp(-B/\beta E)$$

- The constant includes the emitter area
- The gas molecules that get ionised (and allow me this far-fetched assumption!) are indeed the metal vapours created at the tip of the emitters, because of Joule heating by the F-N current.
- It is very difficult to use the full heating model seen before. I made the very crude assumption that the temperature grows with (time)<sup>0.5</sup> and scales inversely with the (thermal conductivity)<sup>0.5</sup>.
- The vapour pressure is then given by:

$$p = p_0 \exp\left(\frac{-H_0}{RT}\right)$$

- Where  $H_0$  is the heat of vaporisation and  $R$  the gas constant.  $p_0$  is a normalisation factor, there is a ratio of approximately  $10^{2.5}$  between Mo and Cu



## Comparison with breakdown rate measurements?

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- All this gives ( $k$  is the thermal conductivity,  $\tau$  the length of the RF pulse):

$$P_{breakdown} \propto I_{FN}(\beta E) * p_0 \exp\left(\frac{-H_0 k^{0.5}}{C \tau^{0.5} J_{FN}^2}\right)$$

- Taking the  $\text{Log}_{10}$ , and applying a single proportionality constant for all the multiplicative factors (only the exponential part of the F-N equation is used):

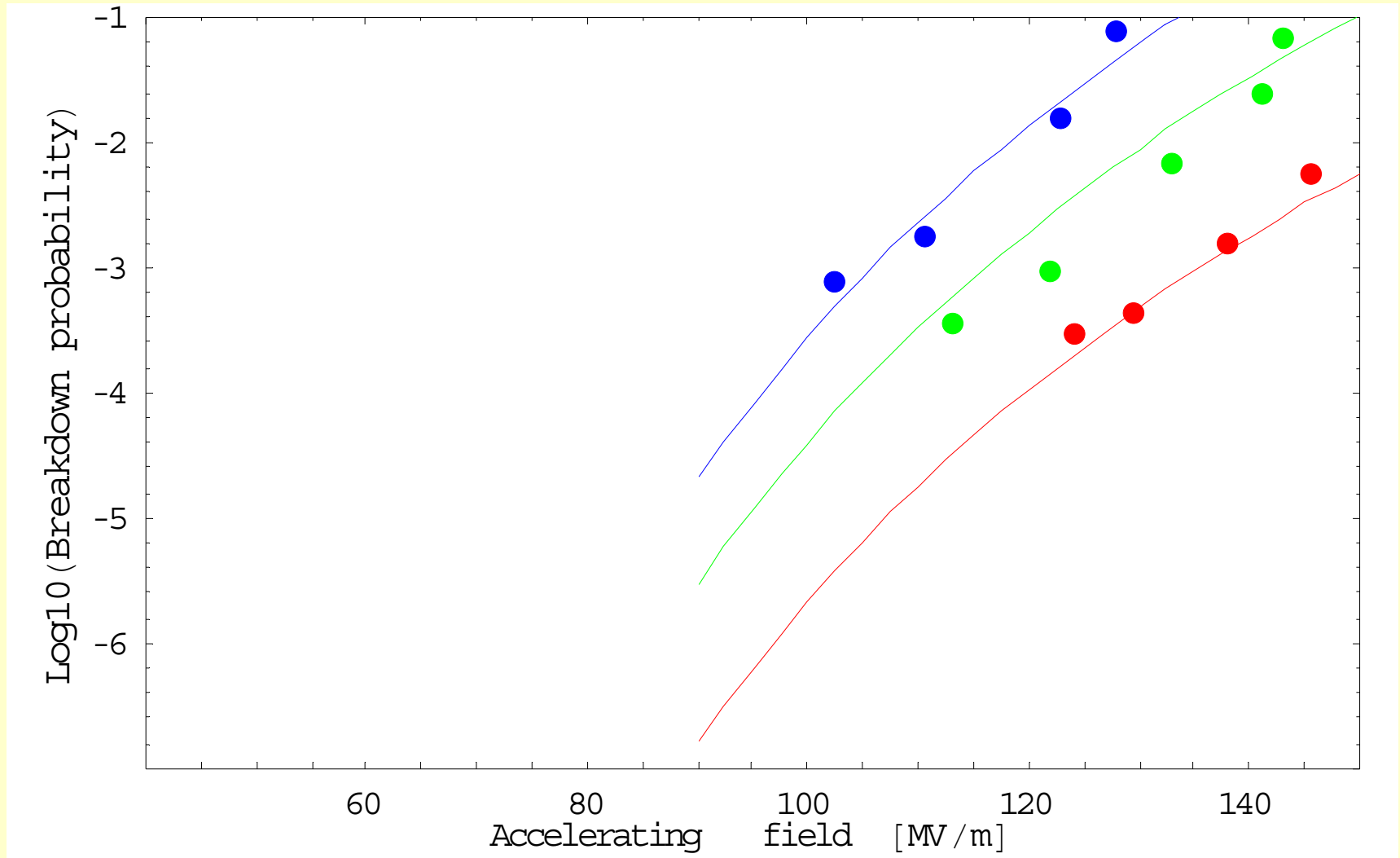
$$\text{Log}(P_{breakdown}) = A + p_0 + 2\text{Log}(\beta E) - \frac{B}{\beta E} - \frac{H_0 k^{0.5}}{C \tau^{0.5} J_{FN}^2}$$

- Where  $A$ ,  $B$ ,  $C$  are fit to the experimental data (and include for example the ionisation cross section, the field emitter area, the probability normalization...)



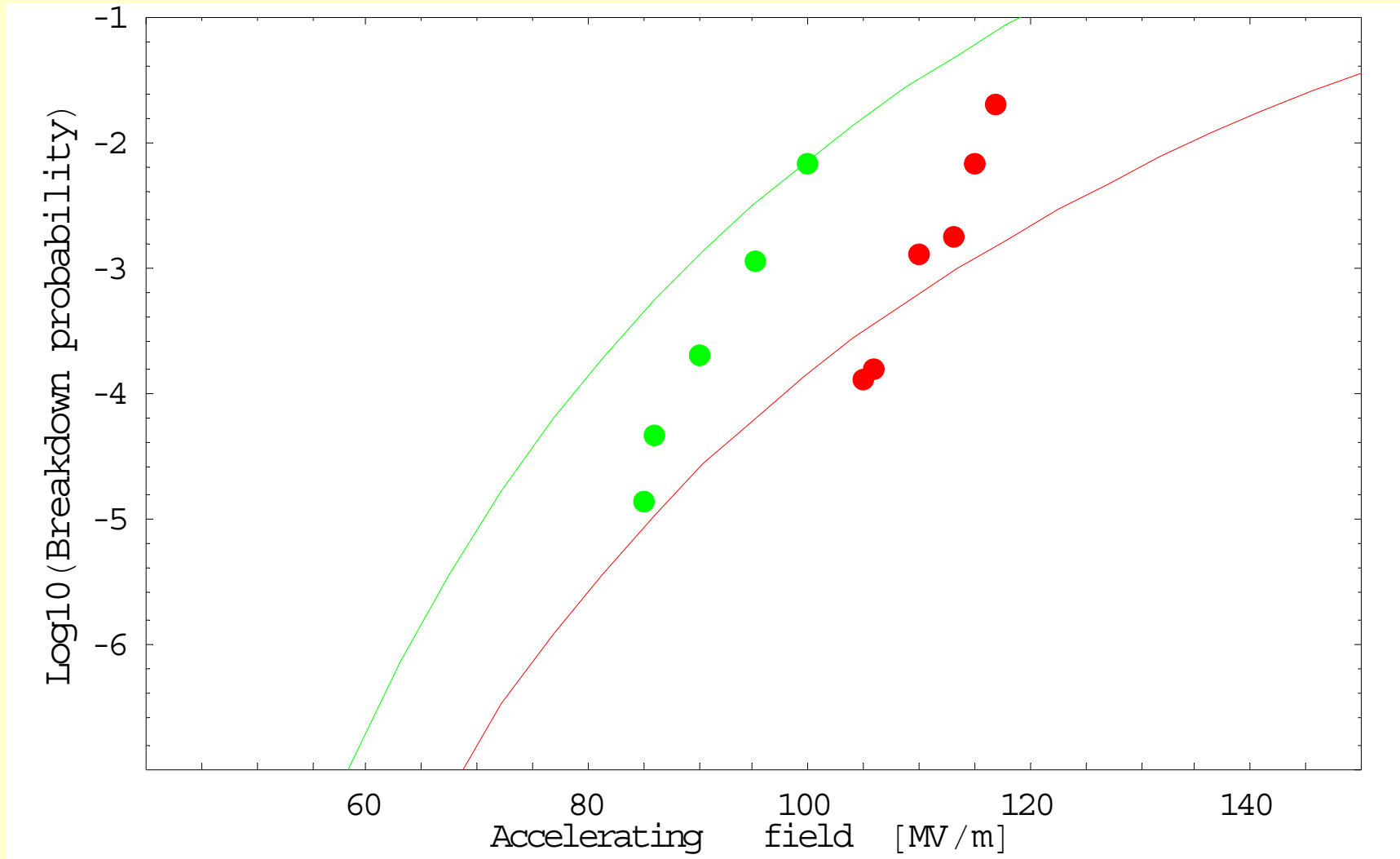
# Fit to Mo data, 30 GHz circular iris

- $\beta = 30$ ,  $k = 138 \text{ Wm}^{-1}\text{K}^{-1}$ ,  $p_0 = 10^{14.5} \text{ mbar}$ ,  $H_0 = 598 \text{ kJ/mol}$



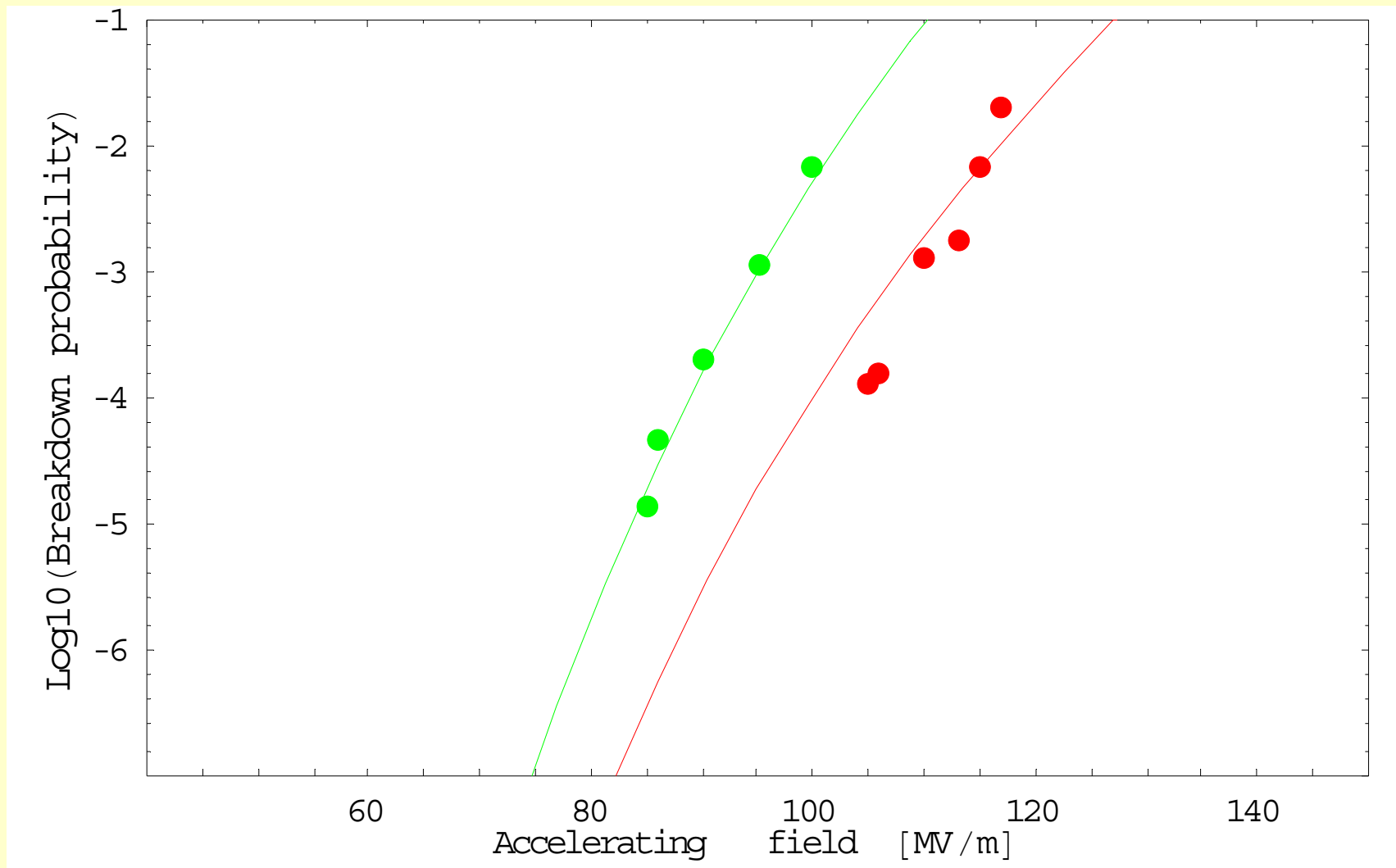
# Keeping the same fit parameters and comparing to Cu data, 30 GHz

- $\beta = 45$ ,  $k = 400 \text{ Wm}^{-1}\text{K}^{-1}$ ,  $p_0 = 10^{12} \text{ mbar}$ ,  $H_0 = 300 \text{ kJ/mol}$ .



# Letting free the F-N fit parameters and comparing to Cu data, 30 GHz

- $B$  doubles and  $A$  increases of 6 units





# Conclusions

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