Test Beam Line (TBL)

Beam Dynamics studies

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The purpose of the TBL

- Validate the drive beam decelerator concept
 - Demonstrate the efficiency of RF power production
 - Demonstrate the stability of the drive beam
 - Demonstrate algorithms and technology for CLIC

Purpose and content of presentation

Purpose of presentation:

"try to outline alignment precision requirements, starting from the energy extraction requirement"

Contents:

- 1. Energy extraction and beam envelope
- 2. Beam stability with transverse wakes (summary)
- 3. Effect of component misalignments

"CLIC" versus "TBL": the graphs and numbers here are for TBL, unless other stated, but the principles are the same for CLIC (one deceleration station)

Part I

Energy extraction and beam envelope

Simulation set-up: LATTICE



The CTF3 drive beam

High-current, low-energy beam for strong wake field generation

Initial beam parameters used for these simulations:

- E₀ = 150 MeV (no energy spread)
- I = 30 A
- d = 25 mm (bunch spacing, f_b = 12 GHz)
- Gaussian bunch, $\sigma_z = 1 \text{ mm}$
- N = 200 (enough for steady-state situation to be reached).

$$\epsilon_{\rm N} = 150 \ \mu {\rm m}$$

Deceleration

- Particles will feel parasitic loss and induce a wake field in the PETS
- The wake field will interact with and further decelerate :
 - 1) rear part of bunch (**single-bunch** effect)
 - 2) following bunches (multi-bunch effect)



 The integrated effect in a PETS on a witness particle due to a source particle is given by (h.o.m. ignored)

$$\int_0^{l_{cav}} F_L(z) ds \approx -q_s q_w w_L(z)$$

where w_L is the std. longitudinal monopole wake function

Simulation software: PLACET

- The simulation package used here is PLACET (D. Schulte)
- Allows to study the effect of single-bunch + multi-bunch wakes precisely
- Beam model used here: sliced beam with a Gaussian longitudinal profile



 wake acting on a given slice is simply the sum contribution from all leading slices (multi- and singlebunch effects treated on equal footing)

Simulation results: energy extraction

PETS longitudinal wake parameters:

- R'/Q = 2294.7 Ω/m (linac-convention)
- f_L=11.99 GHz
- $\beta_{g} = 0.4529$

Beam energy profile after lattice: (initial: flat E₀=150Mev)



NB: start of beam / bunch is to the left! (PLACET output def.)

Wake calculations and group velocity

 The wake is calculated using GdfidL (I. Syratchev), modeled as a single monopole mode traveling out of the PETS with a high group velocity (β_a) [and extracted to HDS]



- In the longitudinal wake function this leads to
 - factor $1/(1 \beta_g)$ (concentration of the field)
 - catch-up distance for the trailing bunch, $s = z\beta_g/(1-\beta_g)$
- The wake parameters R'/Q, β_g and f are taken as input to PLACET the simulation δ-wake:

$$W_{\delta L}(z) = \omega_L \frac{R'}{Q} \frac{1}{1 - \beta_L} \cos(\omega_L \frac{z}{c}) (L - z \frac{\beta_L}{1 - \beta_L}) [V/C]$$

Steady-state

• Catch-up with field from *n* bunches ahead at a distance $s = nd\beta_g/(1 - \beta_g)$

Steady-state energy profile is thus reached after
 n = (I_{PETS}/d)(1-β_g)/β_g = 39 bunches

Steady-state power can be calculated as $P = \frac{\omega}{4v_s} (R'/Q) l^2_{PETS} I^2 F^2(\sigma)$ (P = 172MW, or P ≈ 166MW if wall losses are included)

When the bunch profile and energy extraction efficiency is discussed we always talk about the **steady-state situation**.



Steady state bunch profile

- The steady-state bunch profile depends on the multi-bunch effects as well as the single-bunch effects
- Multi-bunch wake alone would form a symmetrical energy profile (cosine-like wake function, combined with Gaussian distribution)
- Single-bunch wake: last part of the bunch will be more decelerated than the first -> point of minimum energy shifted towards the end
- However, for our case, $n = (I_{PETS}/d)(1-\beta_g)/\beta_g=39$ multi-bunch is dominant



Compare with e.g. profile for CLIC 12 GHz (I_{PETS}= 0.23 m)

Energy extraction efficiency: η

• $\eta = P_{in}/P_{out}$: steady state power extraction eff: $\eta = P[W] \times N / E0[eV] \times I[A]$

Suggestion: it could be useful to express the extraction efficiency as: $\eta = S \times F(\sigma) \times \eta_{dist}$

where for TBL nominal parameters we get:

- S = 63.3 % (max energy spread)
- $\eta = S \times F(\sigma) \times \eta_{dist} = 63.3 \% \times 96.9 \% \times 99.9 \% = 61.3 \%$



(can be changed with detuning: not discussed further here)

The CTF3 drive beam

High-current, low energy beam for strong wake field generation

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- d = 25 mm (f_b = 12 GHz)
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 $\epsilon_{\rm N} = 150 \ \mu {\rm m}$

Resulting parameters:

- P = 166 MW (steady-state power production)
- S = 63.3 % (max .energy spread)
- η = 61.3 % (steady-state extraction efficiency)

Energy spread and beam envelope

Why is the max. energy spread, S, important?
In the TBL we will have the effect of *adiabatic undamping*



The divergence, y'=dy/ds, and thus also the beam envelope will increase with decreasing energy

Calculation of the max. beam envelope

This implies that as the beam is decelerated its transverse size will grow, even without considering transverse wake kicks or machine imperfections

The rms beam size is
$$\sigma_{x,y} = \sqrt{\beta_{x,y}} \varepsilon_{x,y} = \sqrt{\beta_{x,y}} \varepsilon_{N,x,y} / \gamma$$

We define the adiabatic "3-sigma beam envelope" as

 $r_{ad} = \sqrt{3^2 \sigma_x^2 + 3^2 \sigma_y^2}$

where γ is for the lowest energy particle in the bunch

• Setting in for S, with γ_0 the initial gamma we get the value in the middle of a quad:

$$r_{ad} = \sqrt{3^2(\ddot{\beta} + \hat{\beta})\varepsilon_N} / (1 - S)\gamma_0 \approx 3 \cdot 2\sqrt{L_{unit}\varepsilon_N} / (1 - S)\gamma_0$$

For our initial parameters we get

$$r_{ad,after} = 8.3mm, r_{ad,initial} = 5.0mm$$

Meaning: with the nominal paramters cited above we will have a resulting 3σ beam size of 8.3mm due to the adiabatic undamping alone (while half-aperture is a₀=11.5mm) !

Beam envelope along the lattice

Thus, beam envelope along the lattice $r_{ad} \propto 1/\sqrt{\gamma}$, γ for lowest particle



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- N = 200 (enough for steady-state situation to be reached).
- $\epsilon_{N} = 150 \ \mu m$ Initial beam parameters used for these simulations:

Resulting parameters:

- P = 166 MW (steady-state power production)
- S = 63.3 % (max .energy spread)
- η = 61.3 % (steady-state extraction efficiency)

r_{ad} = 8.3 mm (3-sigma envelope due to adiabatic effects alone)

Smaller beam envelope?: reduce the current

- The adiabatic envelope, r_{ad}, can be made as small (large) as we want by decreasing (increasing) the current, I.
- For the TBL, *I* can be calculated on the fly as function of *r*, E_0 , *N* and PETS parameters (only because: $\eta \approx S \times F(\sigma)$, $\eta_{dist} \approx 1$)
- (Calcs omitted)

- However, decreasing the current will mean less power extracted, P, and less extraction efficiency η achieved (while we want to show as high P and η as possible)
- E.g. for if we want a $r_{ad} = (2/3)a_0 = 7.7$ mm we must reduce current to I=27A (with a corresponding lower P=135 W, $\eta = 55\%$)

Challenge: beam dynamics calculations

- We have up to 90% energy spread S (CLIC)
- Spread acts stabilizing (different betatron wavelength lead to decoherence of transverse kicks) – but difficult to calculate the effect
- Also the finite group velocities and damping makes calculations difficult
- No analytical formulas or framework available (ongoing work, try to get somewhere, but no results so far)
- → need for simulations



Part 2

Effect of transverse wakes (summary)

Transverse wakes

• A source particle q_s induces wake fields in PETS cavity



- A witness particle q_w , following at a distance z, is kicked by the fields from leading particles
- The total transverse force on q_w is given by (1D)

$$\int_0^{l_{cav}} F_y(z) ds \approx -\Delta y q_s q_w w_T(z)$$

where $w_T(z)$ is the transverse dipole wake function - the " δ -wake" (h.o.ms ignored here)

PLACET input: dipole wake function

- PETS are modelled with GdfidL (I. Syratchev)
- For a given PETS structure, the transverse $\delta\text{-wake}$ / impedance is calculated



PLACET simulations

- Multiple modes identified from GdfidL calc
- For each mode, $w_{T_i}, Q_i, f_{T_i}, \beta_{T_i}$ are identified
- The total wake function for each mode thus:

$$W_{T_i}(z) = w_{T_i} \sin(\omega \frac{z}{c}) (L - z_{ij} \frac{\beta_T}{1 - \beta_T}) e^{-z\omega/2cQ(1 - \beta_T)} [V/Cm]$$

• Transverse kick of q_w :

$$\Delta y'_w = \sum_{modes} \frac{\Delta p_{y,w}}{m_w c} = \sum_{modes} y_s \frac{q_s q_w}{E_w} W_{\delta T}(z) [rad]$$

Goal: transverse wakes should not amplify beam jitter

- A design target for the PETS is to ensure that beam jitter are not amplified significantly due to transverse wakes (and leading to beam blow-up)
- A number of simulations has been run (initiated by I. Syratchev)
- Results: basically no problem for *nominal* PETS parameters (both CLIC and TBL lattice checked)
- (Example: CLIC low β/high β FODO lattice)





More examples of PETS test simulations

- Metric used: 3 sigma beam envelope at end of lattice
- Initial conditions: beam with initial static offset + jitter at the transverse resonance frequency
- Beam blow-up depends on z/λ_{T_i} : $\sin(\frac{2\pi}{\lambda_{T_i}}z) = 0 \Rightarrow z = \frac{n}{2}\lambda_T \Rightarrow f_T = \frac{n}{2}12GHz$ (zeros)



Part 3

Effect of component misalignment

5 types of misalignment studied





- Now: will study the effect of misalignment of machine components
- Each misalignment (PETS, Quads) studied separately
- 100 random machines simulated for each case. Metric: max. centroid offset, r_c, along lattice (of all machines)
- The initial beam will be assumed to be on the reference orbit
- Adiabatic effect is NOT included in order to study each effect separately (no macroparticles distribution)
- Total 3-sigma beam envelope will therefore be
 - 3-sigma adiabatic envelope "+" centroid envelope : r_{ad} "+" r_c (where the "+" is only in worst case a real +)
- Still: with the adiabatic envelope r=8.3mm (versus half-aperture of a₀=11.5mm) we do not have a large "envelope budget" for component misalignment

1) Position offset of PETS

A PETS off axis will induce transverse kicks (dipole wake ∝ y_{source})
 We scatter the PETS in y: σ_{PETS} = {40 ... 400}µm



(linear graph due to the linear lattice model and same seeds in all simulations - all info in one point)

Prelim. criterion: centroid envelope < 1 mm
 ⇒ σ_{PETS} < 120 μm

Position offset of PETS with Q-scaling

 Also interesting to see effect of large Q in this scenario (previous PETS simulations imply that the effect should not be drastic)



- We see that as long as σ_{PETS} < 100 μm we are still OK, even for a factor Q=3Q₀
- (But this is not "worst case scenario" for PETS: jitter on resonance)

2) Angle offset of PETS

• An angle offset (around x,y) of the PETS centre should basically have the same effect as the corresponding position offset, $\sigma_{\theta-PETS} = (\sigma_{PETS} / 0.5I_{PETS})^{*}2$. Just to confirm:



Prelim. criterion: centroid envelope < 1 mm</p>

 $\Rightarrow \sigma_{\Theta-\text{PETS}} < 0.6 \text{ mrad}$

(An angle offset around s: negligible effect)

3) Position offset of quadrupoles

An offset in a quad will induce a dipole kick
 We scatter the quads in y: σ_q = {10 ... 100}μm



- We see that without any correction of the quad positions we should require a final alignment σ_{PETS} < 10 μm (probably not feasible with prealignment ?)
- Solution: beam-based alignment (BBA)

BBA for quads: 1-to-1 correction

- Quads in TBL (as in CLIC) will be on movers
- The simplest BBA: steer each quad so that the beam goes through centre of the following BPM



- Implementation: correction can in principle be performed in one go. b: BPMs after one pulse. R: the response matrix: \Delta y_c=R+b
- Effectively: quad position error σ_{q_i} is transferred to BPM position error σ_{BPM}
- 1-to-1 correction can be needed as a first correction but we can do better

BBA for quads: dispersion free steering

- The dipole kicks resulting from quad offset will induce dispersion (in the sense "energy-dependent trajectories") in the lattice
- Idea: move quads so that beams of different initial energies follows the same trajectory
- E.g. send the nominal beam with E₀ and a test-beam with E₁=0.8×E₀
- This can, in principle, be implemented by generating the response matrix of both the nominal beam, \mathbf{R}_1 , and for a beam of e.g. lower energy, \mathbf{R}_2 , measure and do the correction $\Delta \mathbf{y}_c = (\mathbf{R}_1 \mathbf{R}_2)^{+(\mathbf{b}_1 \mathbf{b}_2)}$ (weighted against 1-to-1 correction)
- Effectively: quad position error σ_q, is transferred to BPM resolution error σ_{res}

Special variant of DFS needed for TBL

- TBL and CLIC deceleration station:
 - cannot use lower energy beam due to beam stability
 - higher initial energy beam not available
- Trick: we can use a beam with lower current instead Wakefields will be lower and beam will quickly have higher energy
- Can either reduce bunch charge, or take out a number of bunches (probably easier?)

Results seems to be as good as for energy test beam

All results from now are run with optimal DFS weighting

NB: now very easy to test new BBA algorithms in PLACET with then new Octave interface (A. Latina)

Correction with current test beam DFS

 Seemingly very good result (with our linear lattice and ideal elements), and shows the principle

Remains to be studied: the DFS algoritm is, among other things, sensitive to jitter in the main/test beams. E.g. inducing uncorrelated random jitter σ_{beam}=100µm on both beams gives a substantially worse result. However, this can be partially remedied (D. Schulte), but not studied further here.

In the worst case: 1-to-1 correction would give as good result as DFS





TBL as a test-bed for the CLIC station

In any case: it would be very interesting to use the TBL to test the concept of dispersion free steering and other beam-based alignment

 One would like to have similar conditions to the CLIC station (ideally: similar alignment precision and BPM resolution)

TBL: also test-bed for automation of BBA ?

4) Angle offset of quadrupole

- A small rotation around s (skew quadrupole) will have negligible effects for the 8 FODO cell lattice in question
- A small rotation around x, y will have negligible effect (integrated force ≈0, due to negligible motion in a quad)
- Quad angle offset in y: $\sigma_{\theta q} = \{0 \dots 2\}$ mrad. Just to confirm:



Negligible for even relatively large rotation

Wrap-up: full simulation

We now put errors on all elements simultaneously, in both x and y

{σ_{PETS}, σ_{θ-PETS}, σ_q, σ_{BPM}}, (100,200) um (or corresponding angle)
 This time we observe the *total* 3-sigma beam envelope, r_{ad} "+" r_c (w and w/o correction)



Now: with Q=2Q₀



Discussion

Trustworthiness of the simulation results

"Are we now sure to get the TBL beam through???"

- In "favour"
 - Our metrics are conservative
- In "disfavour"
 - several important idealizations:
 - Iattice: except scattering and BPM res: ideal lattice elements
 - lattice: linear lattice
 - beam: Initial 0 bunch energy spread
 - beam: gaussian bunch shape
 - wakes: Only monopole and dipole wake
 - wakes: PETS Q factor difficult to predict
 - ...and more
- First conclusion: a TBL is still needed...

Conclusions

The nominal PETS parameters given seem satisfactory

- We see that the difference between a position accuracy of $\sigma = 100 \ \mu m$ and $\sigma = 200 \ \mu m$ is significant
- Under the conditions in these simulation, with σ = 200 μm we cannot get the beam fully through even when doing 1-to-1 correction (only with perfect DFS steering) (without reducing I, P and η)

• The margin for σ = 100 μ m is much more comforting. Ideally :

- $\Rightarrow \sigma_{PETS} \leq 100 \ \mu m$ (minimize transverse wake kick)
- $\Rightarrow \sigma_{\theta\text{-PETS}}$ <= 0.5 mrad (same reason)
- $\Rightarrow \sigma_{quads} < =100 \ \mu m$ (get beam through in order to prepare for further corrections)
- $\Rightarrow \sigma_{\text{BPM}}$ <= 100 μm and σ_{res} <= 5 μm
- \Rightarrow Mover positioning resolution in x and y: same O.M. as σ_{res}