

# DC spark experiments for CLIC : test of new materials, heat treatments and breakdown rate measurements

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TS-MME

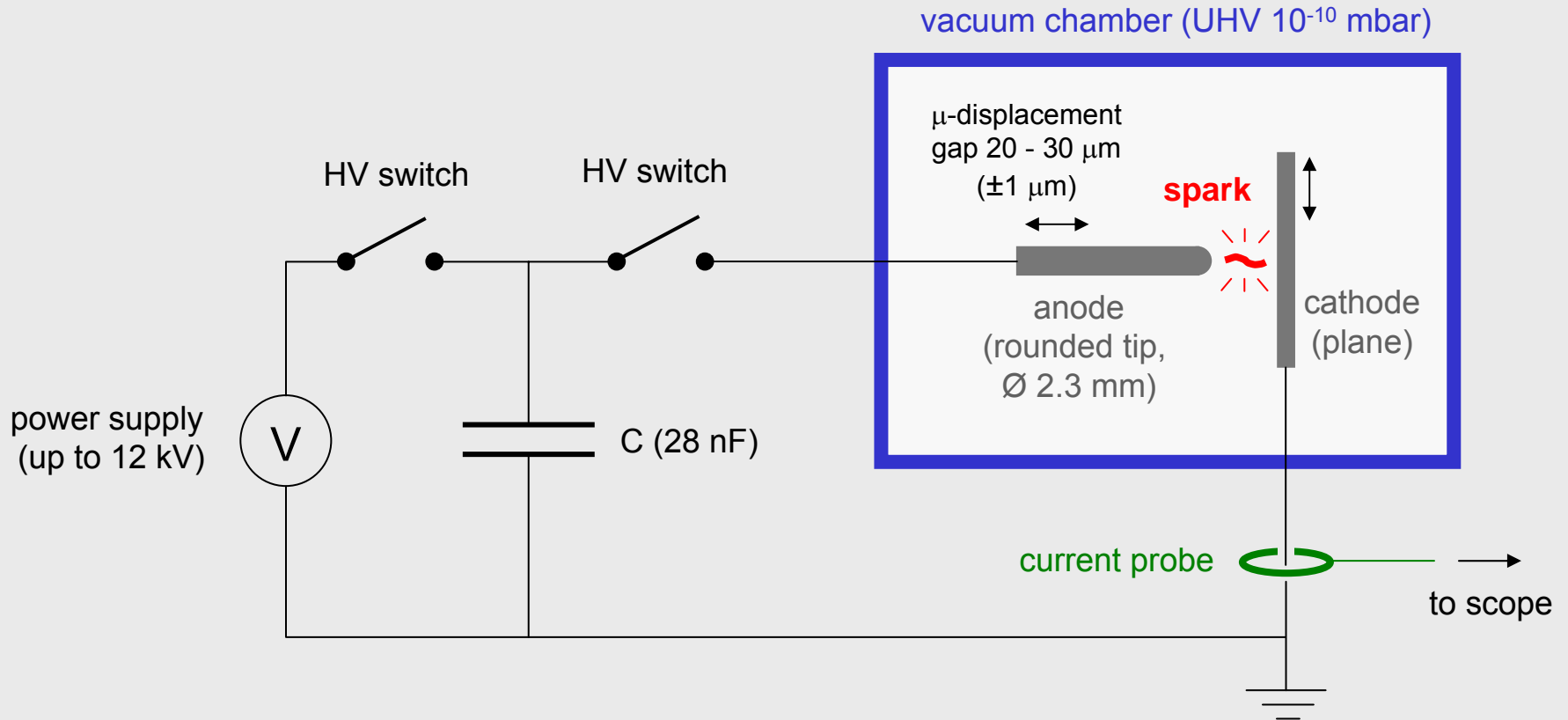


CLIC meeting  
2<sup>nd</sup> november 2007

# Outline

- Experimental setup
- New materials tested (since last presentation by Trond, in january 07)
- Heat treatments of Mo and Cu in oven
- Breakdown rate results
- Conclusions

# Experimental set-up



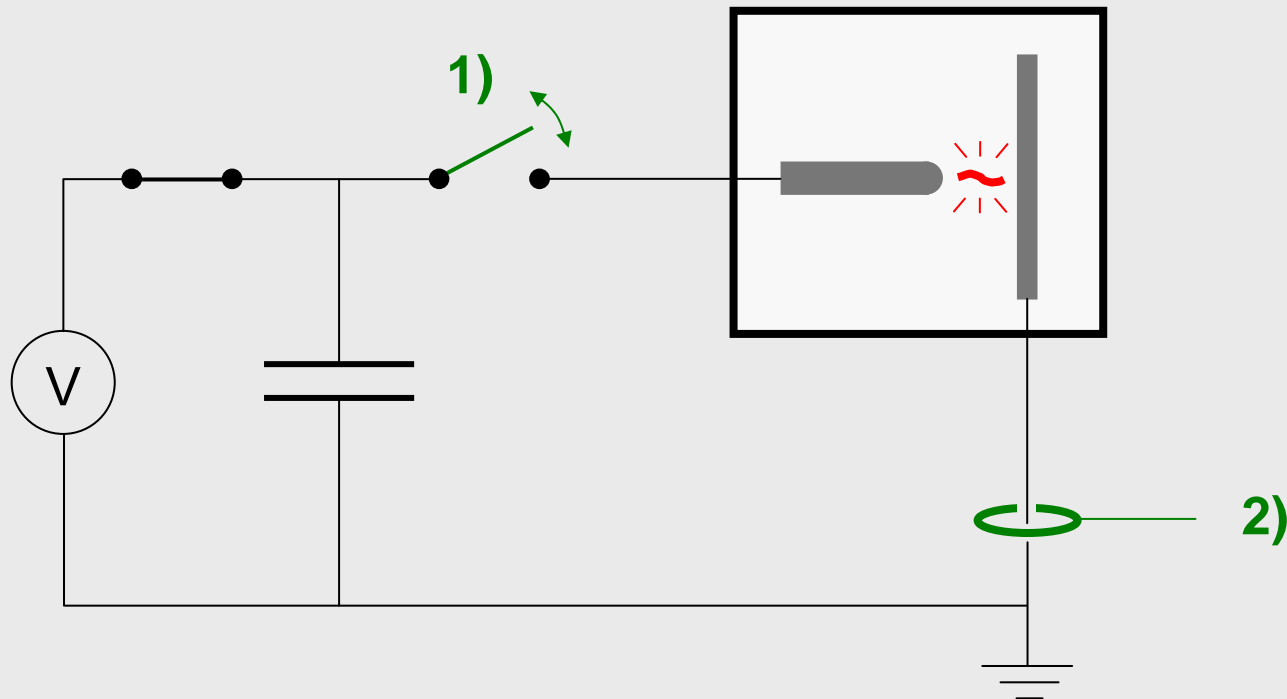
- max. field :  $12 \text{ kV} / 20 \text{ } \mu\text{m} = 600 \text{ MV/m}$
- typ. spark energy :  $\frac{1}{2} \cdot (28\text{nF}) \cdot (10\text{kV})^2 = \sim 1 \text{ J}$

# Types of measurement

A) Field emission  $\rightarrow \beta$

B) Breakdown field  $E_b \rightarrow$  conditioning curve, saturated field  $\bar{E}_b$

 C) Breakdown rate  $\rightarrow$  breakdown probability vs field



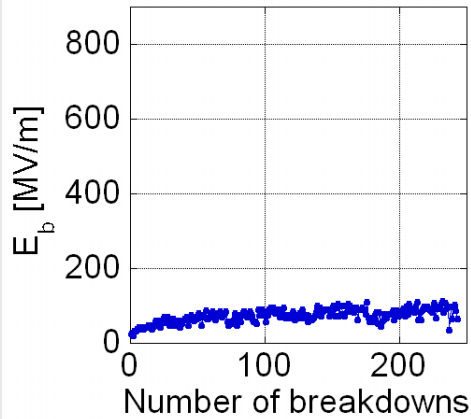


# Outline

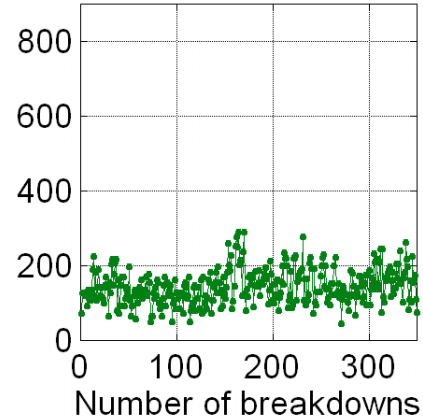
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# Conditioning curves of pure metals

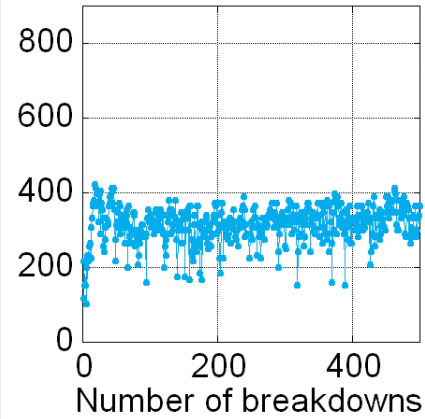
**C**



**Cu**

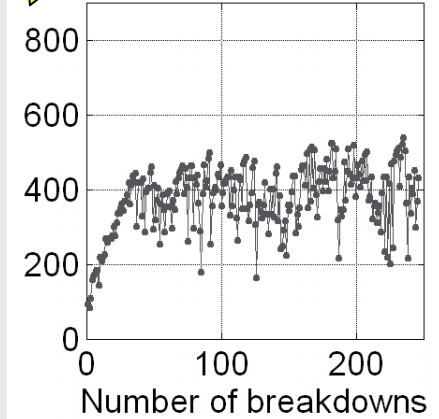


**W**

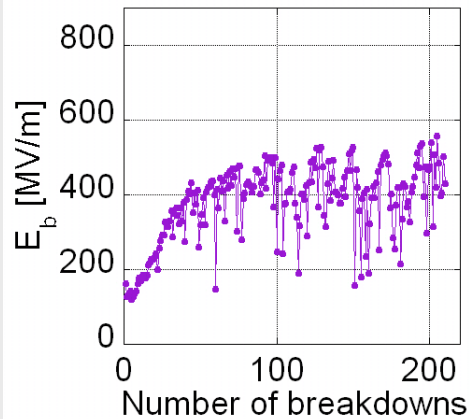


**NEW!**

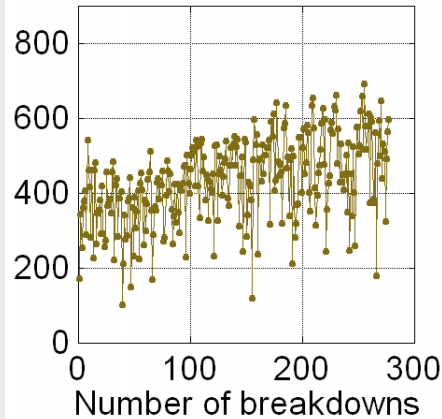
**Nb**



**Mo**

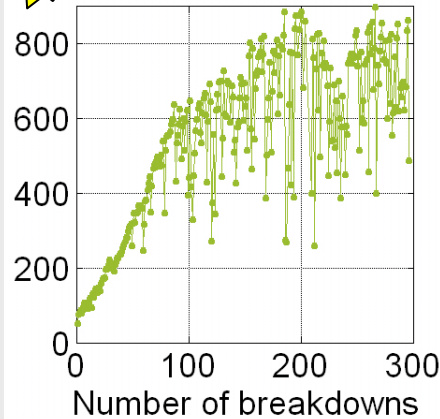


**Cr**

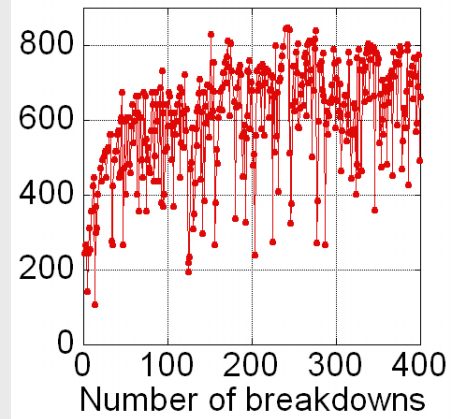


**NEW!**

**V**



**Ti**

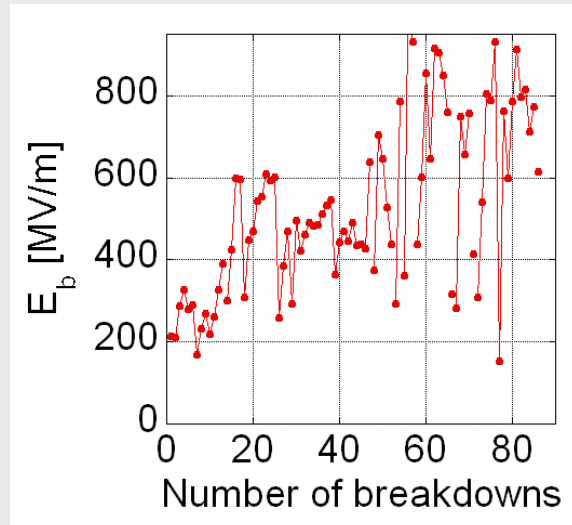


assumption: 'good material' = refractory ; oxides easily reduced

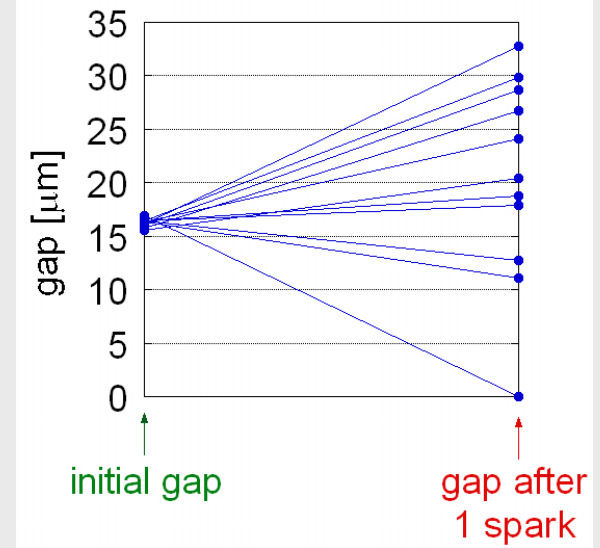
# Alloys

- Ti – 15% Mo

Thanks to PX Group and to Gonzalo for the sample.

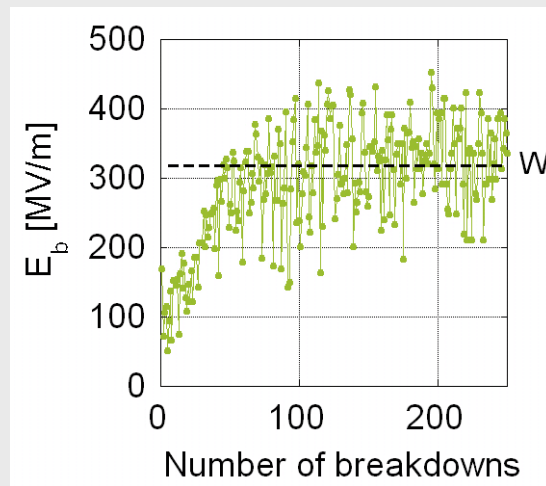


gap highly unstable!




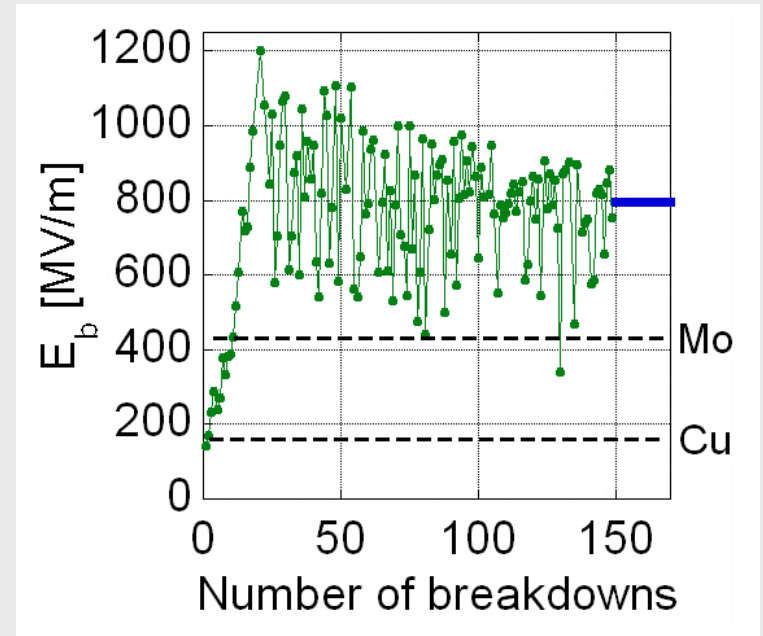
- Tungsten carbide (10% Co)  
(tests are running now)

Thanks to DIXI Polytool and to Gonzalo for the sample.



# Stainless Steel (316LN)

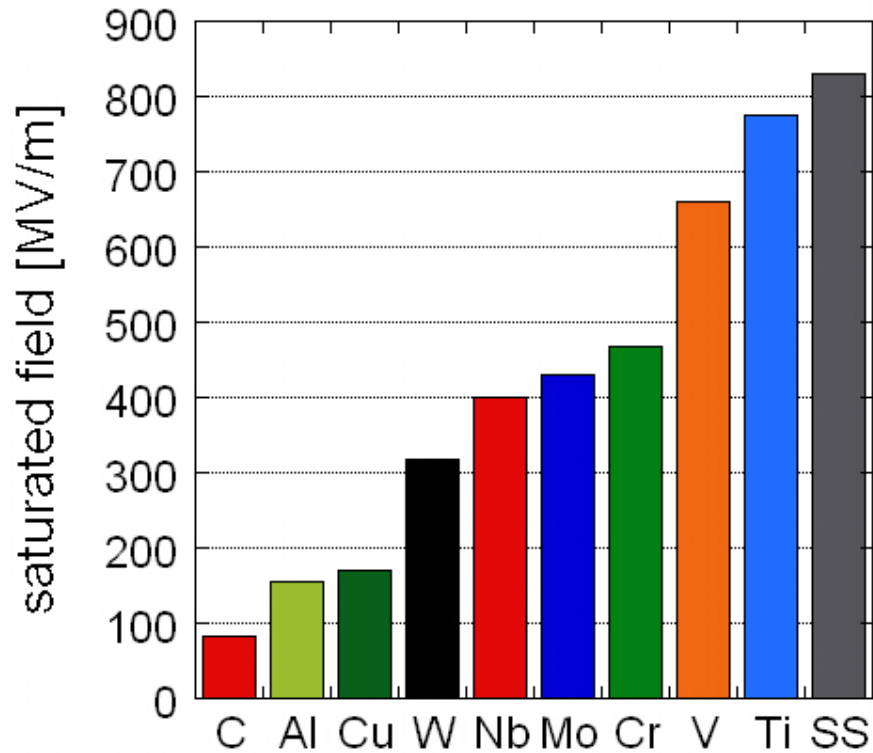
- very high saturated field
  - $\bar{E}_b = 830 \text{ MV/m}$  
- fast conditioning speed
  - 20 sparks
- gap quite stable (similar to Mo, Cu)
- very small beta value after conditioning
  - $\beta \approx 6$
- large standard deviation ( $E_b$ )
  - $\sigma \approx 200 \text{ MV/m}$
- Such high fields are critical for this setup!
  - gap  $\approx 9 \text{ }\mu\text{m}$ , really small...



	$\bar{E}_b$ [MV/m]	$\langle \beta \rangle$	$\beta E_b$ [GV/m]
Cu	170	46	7.8 ( $\pm 1.3$ )
Mo	430	16	6.9 ( $\pm 1.9$ )
SS	830	6	5 ( $\pm 1.4$ )

➔ SS: low conductivity. Add Cu coating ?

# Ranking of materials



## • conditioning speed



Cu	“immediate”
SS	~ 20 sparks
Mo, Ti	~ 50 sparks
V	~ 100 sparks

## • gap instability



Mo	< 15 %
Cu, SS	< 25 %
Ti	< 50 %

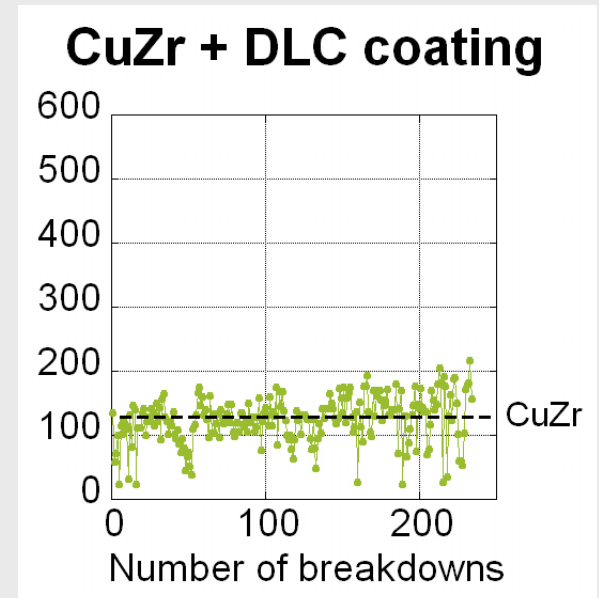
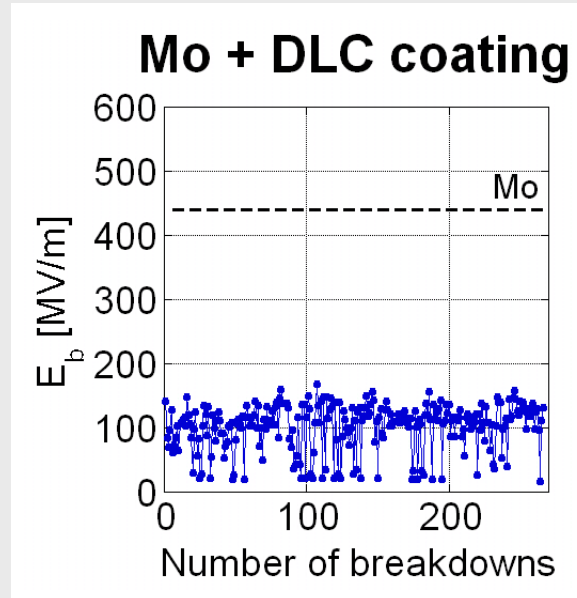
(max. gap variation after a full conditioning experiment)

- broad range: 100 – 1000 MV/m
- difficult to point out 1 dominant physical property, combination of several ones  
(melting point, heat of fusion, thermal conductivity, electrical conductivity, vapour pressure, surface tension, work function, ...)

# Other materials

- Metals with 2  $\mu\text{m}$  DLC coating  
(idea: increase thermal conductivity to evacuate heat)

*Thanks to DIARC and to Samuli for the samples.*



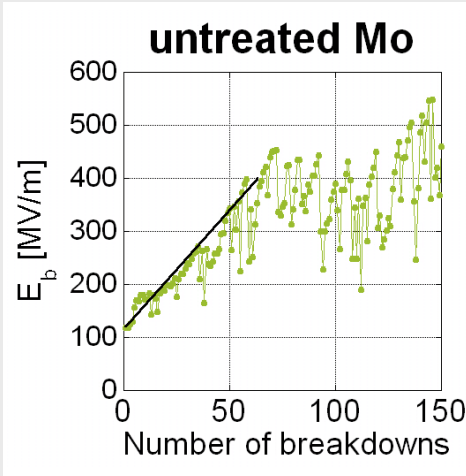
- ready to be tested : Ta  
Cu + Cr coating  
'home-made' Ti-Mo  
Mo, W machined with EDM  
chemically polished Cu

# Outline

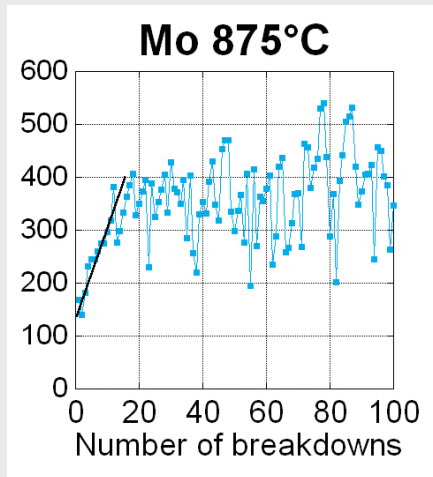
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# Ex-situ heat treatment in oven (Mo, 2h)

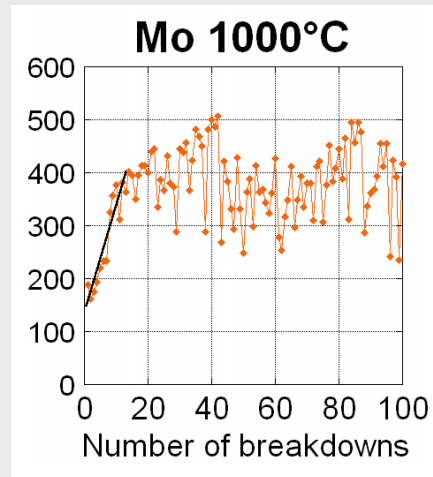
Thanks to Ivo Wevers  
for the treatments.



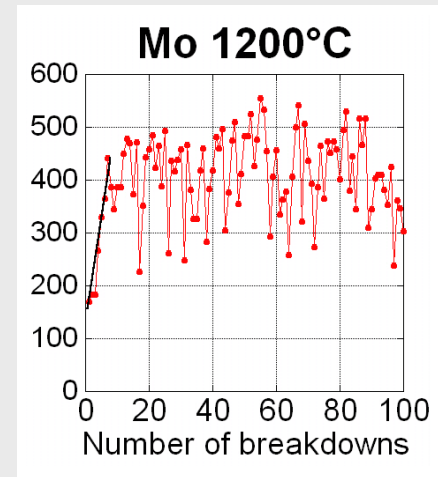
~ 60 sparks  
(to reach 400 MV/m)



~ 15 sparks



~ 12 sparks



~ 10 sparks

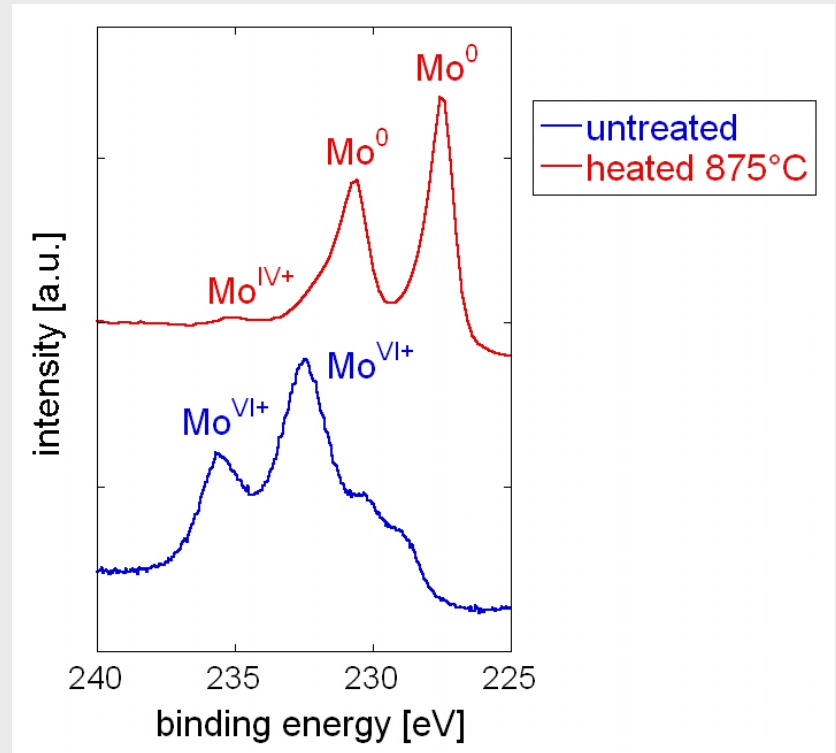
→ same saturated field, conditioning speed improved



# Ex-situ heat treatment in oven (Mo, 2h)

- XPS measurements :

Amount of Mo oxides at the surface reduced after heat treatment



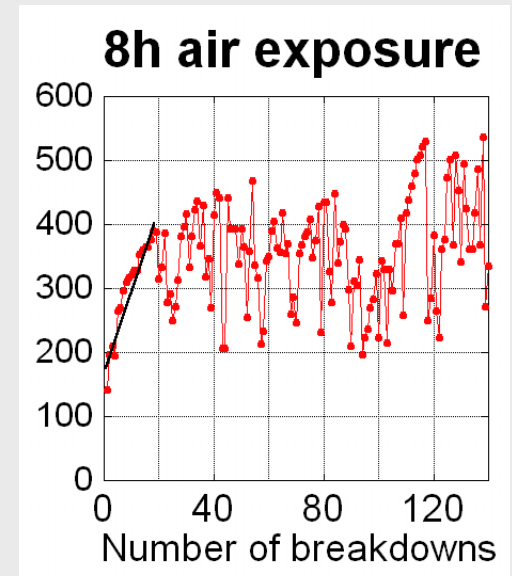
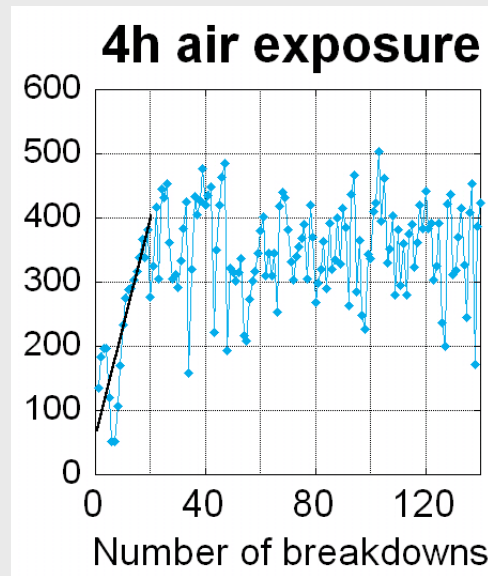
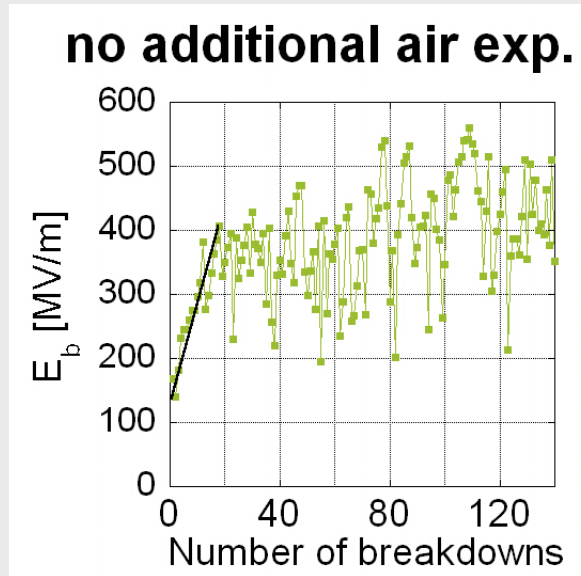
- Hardness measurements : 1000°C and 1200°C samples are recrystallized, 875°C sample is **not** recrystallized

*Thanks to Alex Gerardin  
for the measurements.*

→ conditioning speed improved by oxides reduction  
2h at 875°C is a good choice (to be tested soon on RF structures)

# Effect of dry air exposure after heat treatment (Mo 875°C)

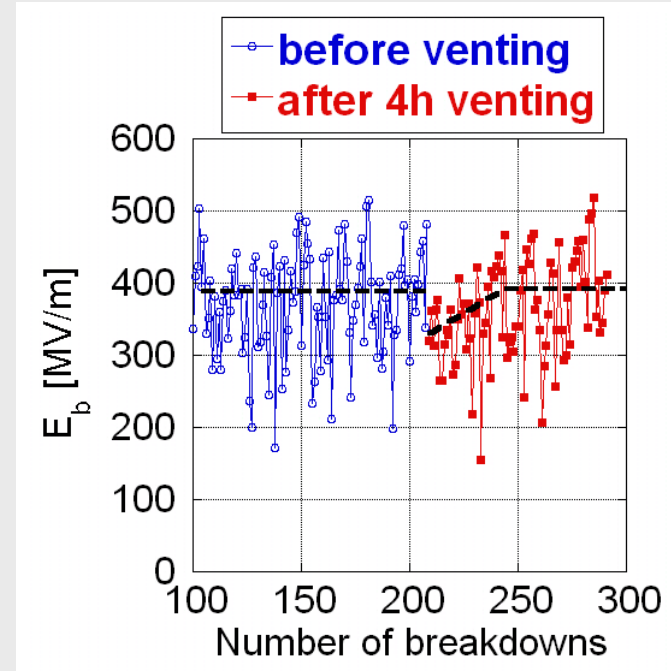
- no significant degradation on virgin spots after 8 hours exposure (~ mounting time of structures in CTF)



- confirmed by XPS : oxidation still negligible after 8h air exposure

# Effect of dry air exposure after heat treatment (Mo 875°C)

- small degradation on conditioned spots after 4 hours exposure

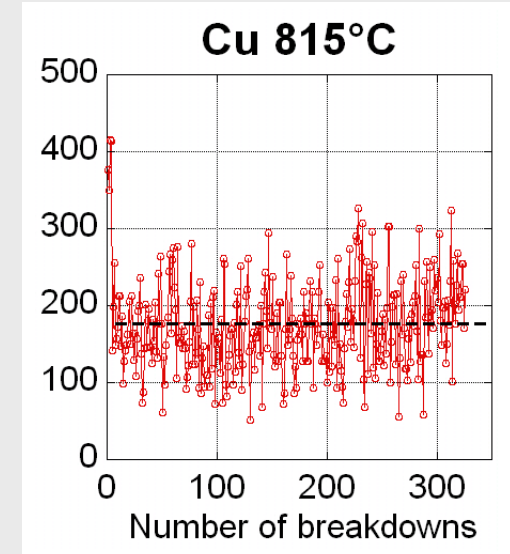
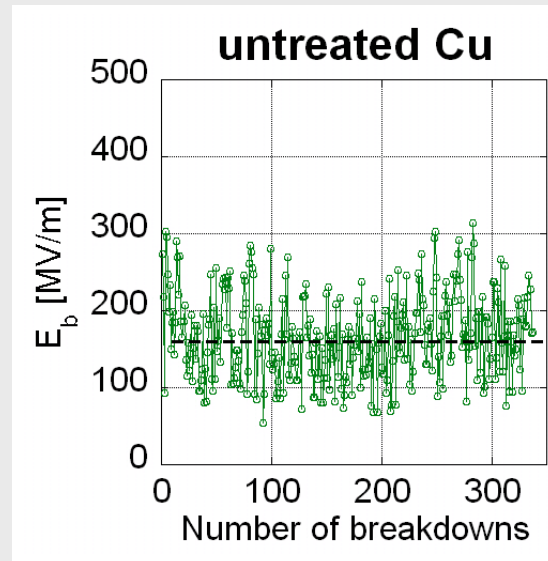


→ conditioned spot : more reactive to oxide formation

# Ex-situ heat treatment in oven (Cu, 2h)

- Slight improvement in saturated field (10%)

*Thanks to the brazing team for the treatment.*



- Saitama University results (1996)

Kobayashi *et al.*, Vacuum **47** 745 (1996)

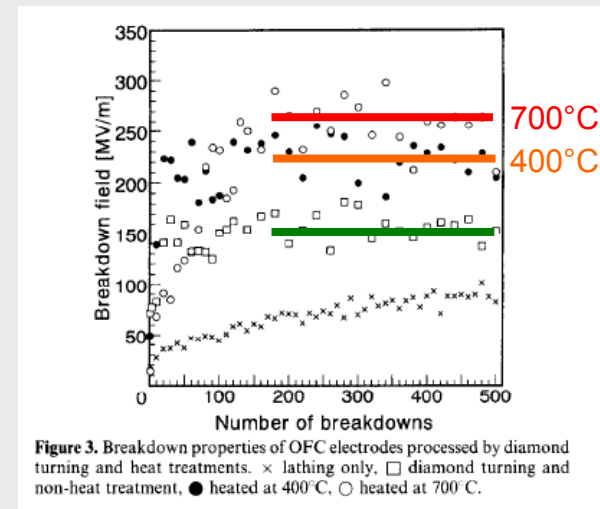


Figure 3. Breakdown properties of OFC electrodes processed by diamond turning and heat treatments. × lathing only, □ diamond turning and non-heat treatment, ● heated at 400°C, ○ heated at 700°C.

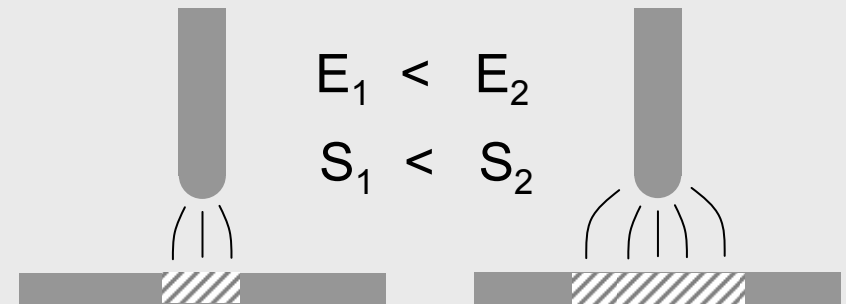
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# Breakdown rate : procedure

1. conditioning of the spot
2. find field for BDR = 1
3. to reach lower BDR, decrease field by 25 MV/m steps at least  
( $\approx$  max. variation in E due to gap changes during 1 run, max. 'precision' in E)

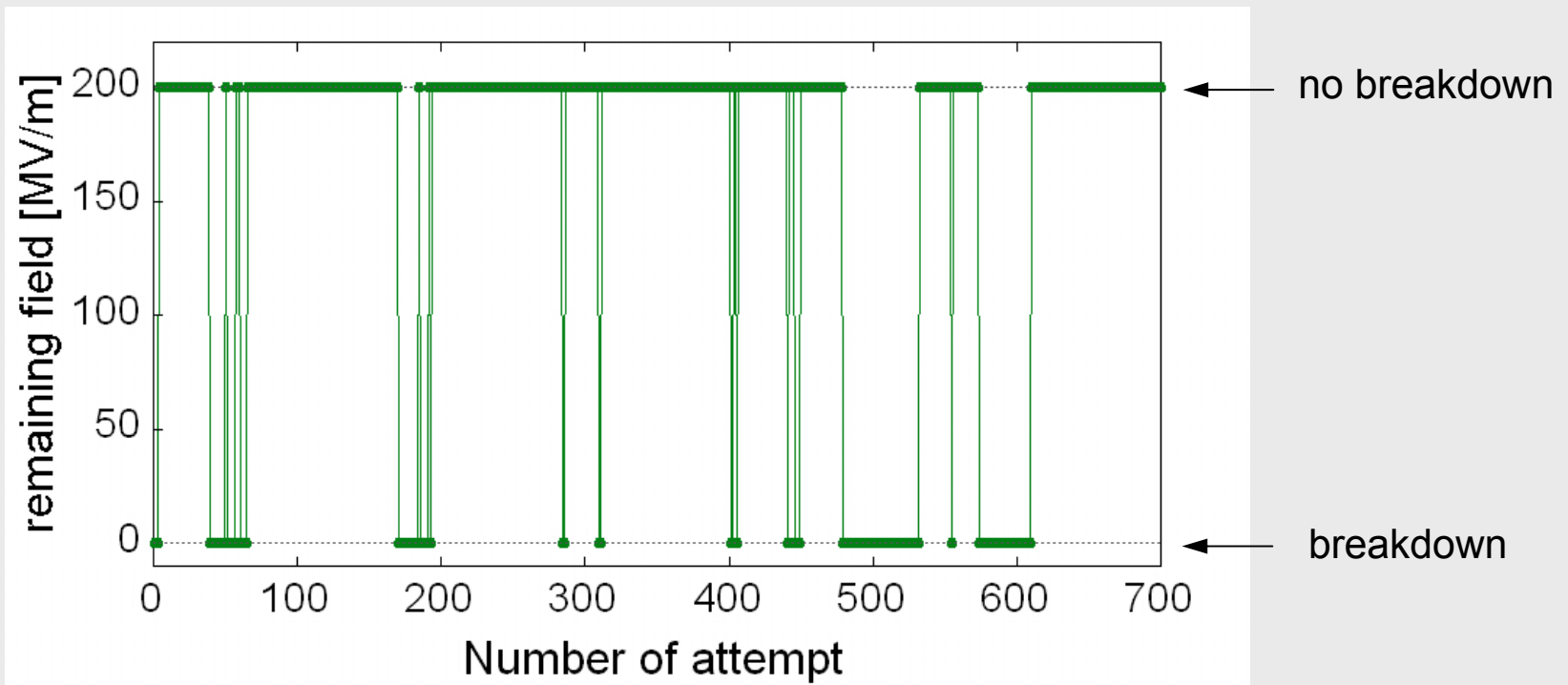
- works not well by increasing E :  
sparks mostly grouped at the beginning of the run (due to emitters located in the 'uncleaned' area?)



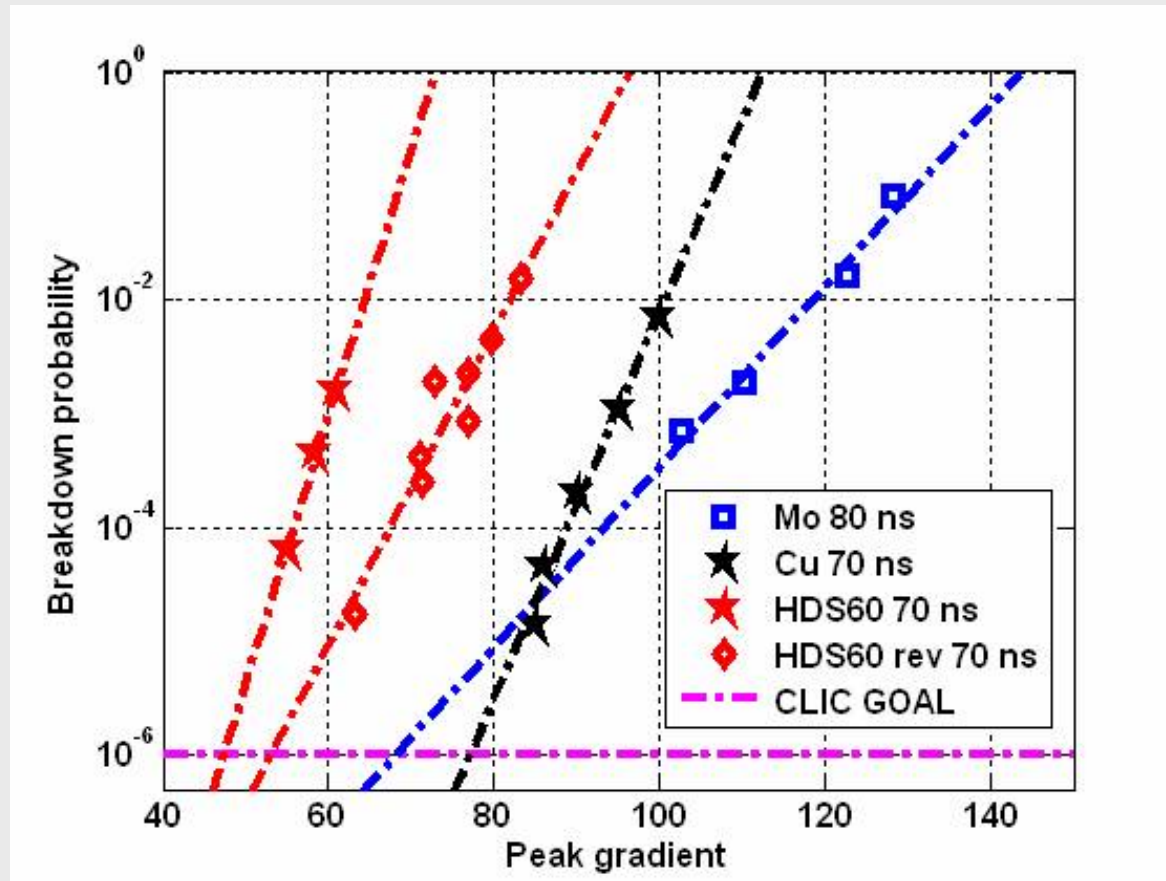
- $\sim 6$  sec / attempt
- experimentally difficult to go under a breakdown probability of  $10^{-4}$   
(time consuming, poor statistics, frequent mechanical problems with HV switch)

# Breakdown rate : sparks distribution

- breakdowns are randomly distributed, but come often by groups



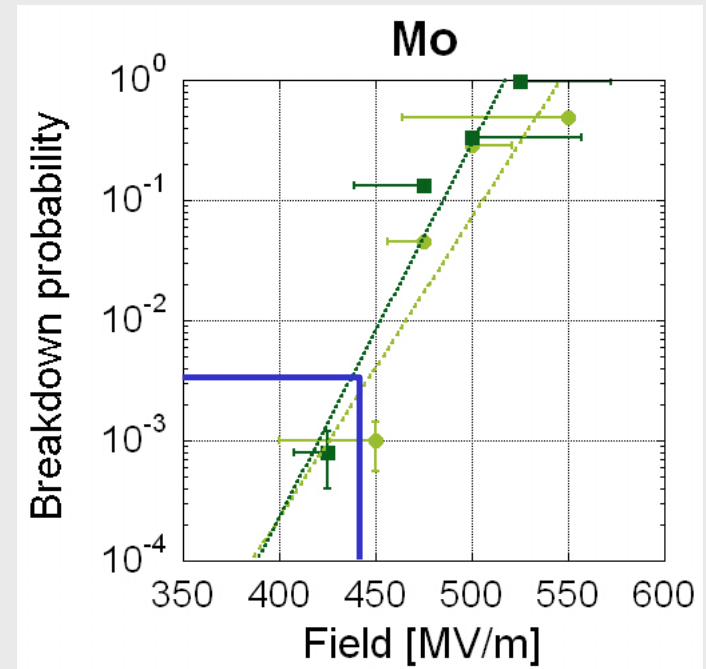
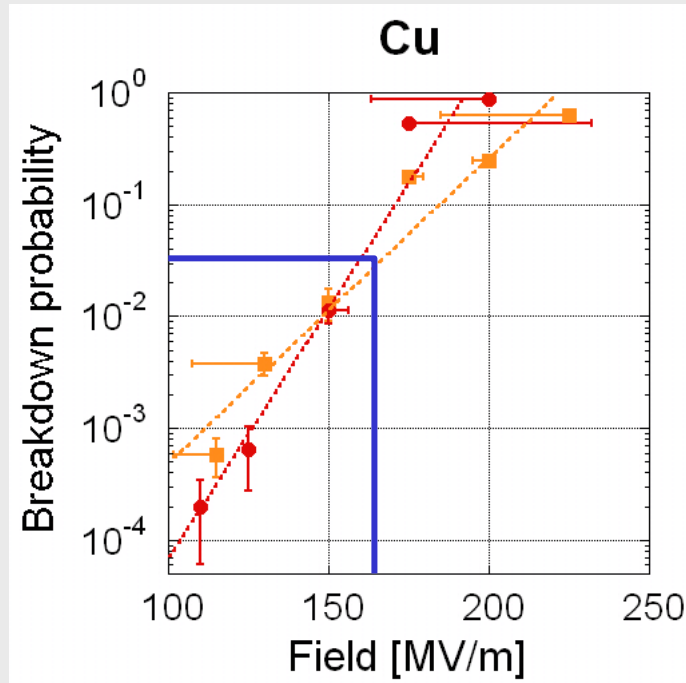
# Breakdown rate vs field : RF (30 GHz)



→ Points are aligned in a  $\log(P)$  vs  $E$  plot. **And in DC ?**

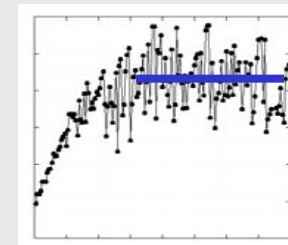


# Breakdown rate vs field : DC

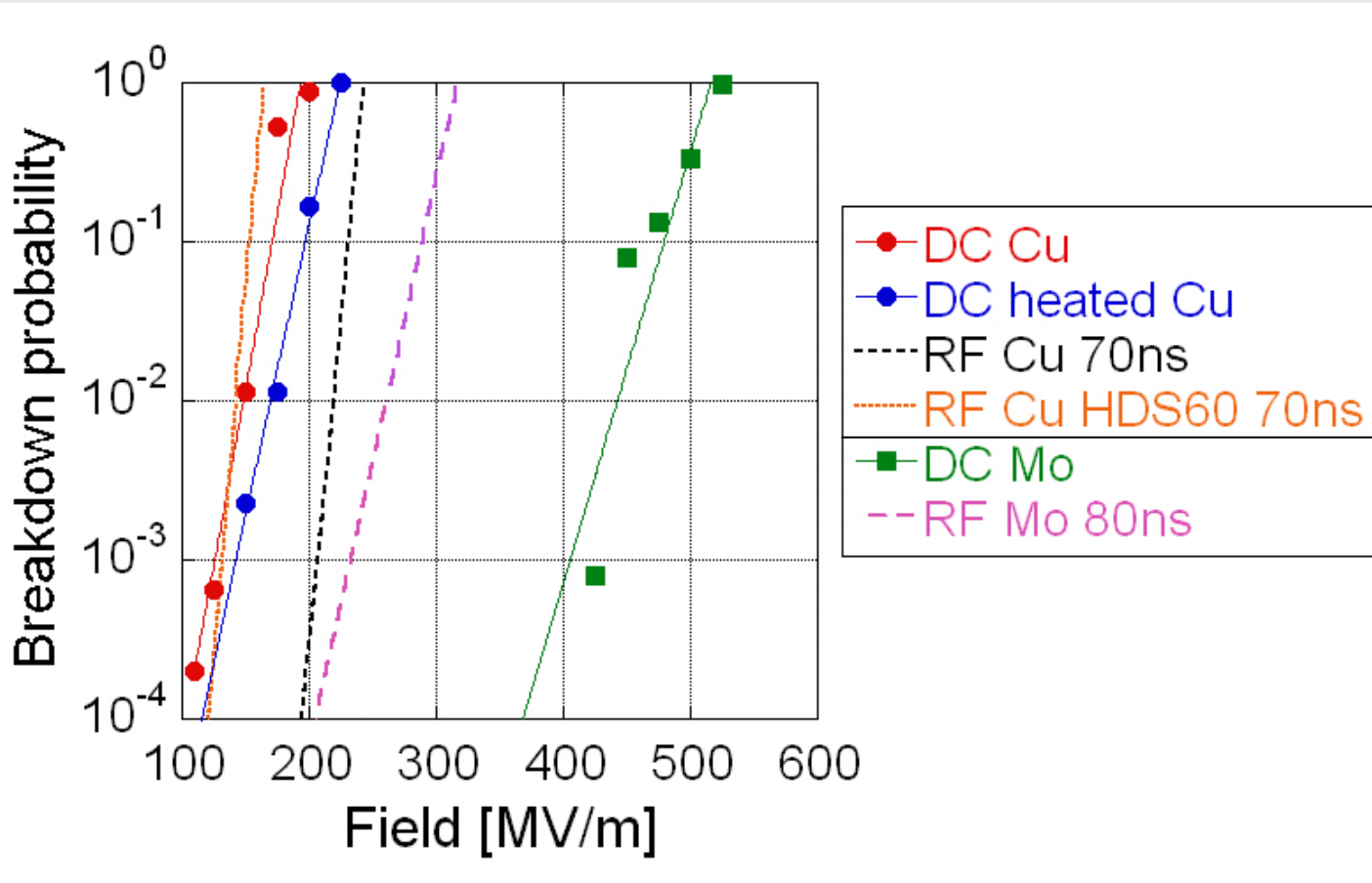


Same trend as in RF measurements → comparison possible

NB: low BDR @ saturated field ( $\sim 10^{-2}$ )



# Breakdown rate vs field : RF & DC (1<sup>st</sup> version)



absolute slope:  
1 decade every...

**28 MV/m** (±6)

**27 MV/m** (±3)

**13 MV/m**

**11 MV/m**

**37 MV/m** (±5)

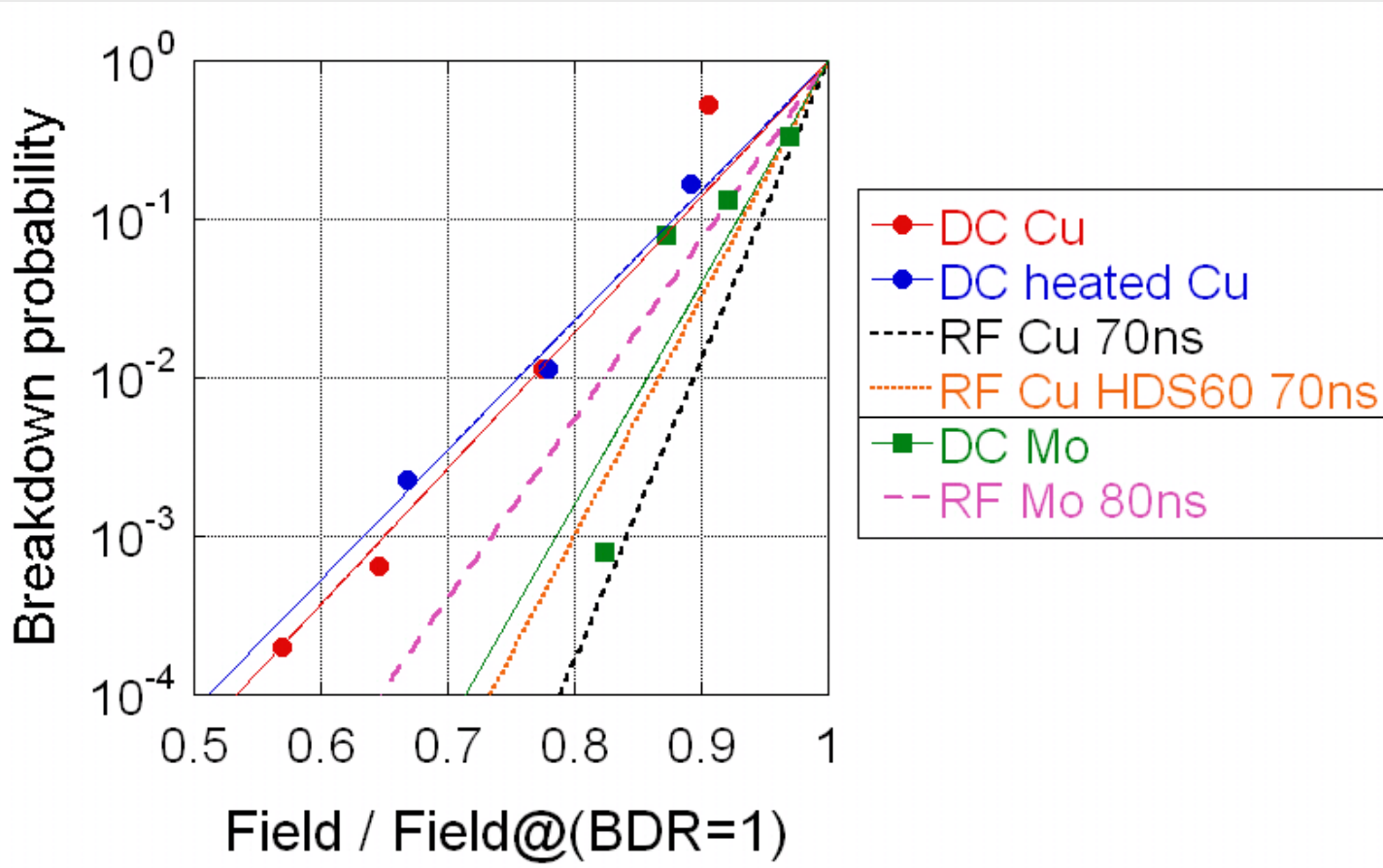
**28 MV/m**

NB: RF data are plotted vs surface field



RF & DC slopes are different  
Cu steeper than Mo in both cases

# Breakdown rate vs field : RF & DC (2<sup>nd</sup> version)



slope:  
# decades over 20%  
of field@(BDR=1)

1.7 ( $\pm 0.4$ )  
1.6 ( $\pm 0.1$ )  
3.8  
3  
-----  
2.8 ( $\pm 0.4$ )  
2.3

Normalization : 'how many decades do we gain if we decrease the max. field by X%'



RF & DC slopes are different for Cu, similar for Mo  
Mo steeper than Cu in DC

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# Summary

- Various metals and alloys have been tested ( $E_b$ , cond speed, gap stability)
  - Stainless Steel : highest saturated breakdown field, gap stable
  - difficult to understand the ranking of materials...
- Heat treatment of Mo
  - increase in conditioning speed by removing oxides
  - no deterioration after 8h air exposure
- Heat treatment of Cu
  - slight increase in saturated field
- DC breakdown rate measurements
  - Breakdown probability increases exponentially with applied field
  - DC – RF : different slopes, Cu steeper than Mo (?)

# Outlook

- Continue tests of materials, coatings & surface preparation
- More breakdown rate
- Optical Emission Spectroscopy of the spark (feedthrough with optical fiber)
  - composition, temperature, density
  - pre-breakdown
- 2<sup>nd</sup> DC spark system will run in a few weeks...

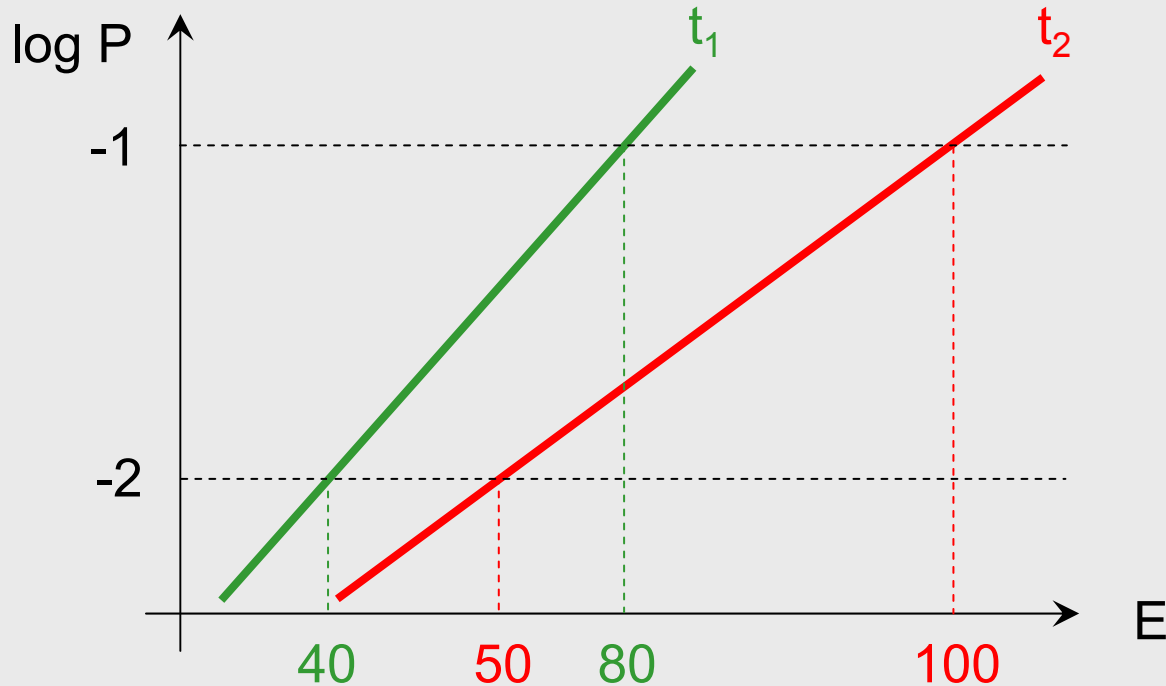
*lots of work done by Yngve Levinsen*

- up to 30 kV
- energy of sparks can be changed
- run BDR and tests of materials in parallel

**Thank you !**

# Slope ?

- Schematic pulse length dependence in RF (same structure)



$$\frac{1 \text{ dec.}}{(100 - 50)} \neq \frac{1 \text{ dec.}}{(80 - 40)}$$

$$\frac{1 \text{ dec.}}{\frac{(100 - 50)}{100}} = \frac{1 \text{ dec.}}{\frac{(80 - 40)}{80}}$$



absolute slope is not relevant  
normalize fields by field at a fixed BDR



# Materials properties

	sat. brkd field MV/m	melting point °C	boiling point °C	heat of fusion J/mm <sup>3</sup>	heat of evaporation J/mm <sup>3</sup>	thermal conductivity W/mK	electrical conductivity 10 <sup>8</sup> Ohm <sup>-1</sup> m <sup>-1</sup>	vapor pressure at melt. point Pa	vapor pressure at 1080°C Pa	vapor pressure at 1680°C Pa	surface tension	density kg/m <sup>3</sup>	Z	work function eV
<b>Cu</b>	170 (7)	1083 (9)	2567 (8)	1.8 (7)	42 (7)	401 (1)	59.6 (1)	0.05 (1)	5E-2 (8)	2E2 (7)		8920	29	4.65
<b>W</b>	315 (6)	3410 (1)	5660 (1)	3.7 (1)	87 (1)	174 (2)	18.9 (2)	4.27 (7)	4E-21 (1)	7E-11 (1)		19350	74	4.55
<b>Nb</b>	400 (5)	2468 (4)	4742 (3)	2.4 (4)	63 (3)	53.7 (6)	6.9 (6)	0.075 (2)	1E-15 (3)	4E-7 (3)		8570	41	4.3
<b>Mo</b>	440 (4)	2617 (3)	4612 (4)	3.4 (2)	63 (3)	138 (3)	18.7 (3)	3.47 (6)	2E-13 (4)	1E-5 (4)		10200	42	4.6
<b>Cr</b>	470 (3)	1857 (6)	2672 (7)	2.3 (6)	48 (6)	93.7 (4)	7.7 (4)	990 (8)	7E-3 (7)	4E2 (8)		7200	24	4.5
<b>V</b>	660 (2)	1890 (5)	3380 (5)	2.4 (4)	53 (5)	30.7 (7)	4.9 (7)	3.06 (5)	8E-8 (5)	1E-1 (5)		5960	23	4.3
<b>Ti</b>	780 (1)	1660 (7)	3287 (6)	1.5 (8)	40 (8)	21.9 (8)	2.3 (8)	0.49 (3)	2E-6 (6)	5E-1 (6)		4540	22	4.33
<b>SS</b>	830	~1510 (8)				15	1.3					7950	-	
<b>Ta</b>	?	2996 (2)	5425 (2)	2.9 (3)	68 (2)	57.5 (5)	7.6 (5)	0.77 (4)	1E-19 (2)	1E-10 (2)		16600	73	4.25
<b>WC</b>	310	2780	6000			84	1.4					14450	-	