









# Motivations

# Another six 3 GHz RF pulse compression systems are required for CTF3 nominal operation.





Barrel cavity short theory.



Cavity profile

$$z = \sqrt{ar_0 \left\{ 1 - \left(\frac{r}{a}\right)^2 \right\}}$$

The eigen-frequency of the Barrel cavity with  $E_{mng}$  oscillation is the solution of the next equation:

$$ka = v_{mn} + \frac{(q-1/2)\alpha}{\sin\theta}$$

 $v_{mn}$  is a root of the Bessel function that for the big *m* can be approximated as:

$$v_{mn}^{o} = m - \mu t_{n}^{0}$$
  $(n = 1, 2, ...),$   
 $-t_{n}^{0} = [(n - 0.25)1.5\pi]^{2/3}, \quad \mu = \left(\frac{m}{2}\right)^{1/3}$ 

The optimal radius  $r_0$ , when the external caustic has the smallest height comes from:  $r_0 = 2a \sin^2 \theta$ where  $\alpha$  and  $\theta$  are derived from:

$$\sin \alpha = \sqrt{\frac{a}{r_0}} \sin \theta$$
  $\cos \theta = \frac{m}{v_{mn}}$ 

Finally the height of the external caustic and Q-factor of the cavity are:

$$z_{q-1} = 2\sqrt{(q-1/2)\frac{a\sin\theta}{k\sin 2\alpha}}$$

$$Q_E = \frac{a}{\sigma_s}$$







Whispering Gallery Mode Fields patterns

~ 0.6 m





Whispering Gallery Mode:  $TM_{10,1,1}$ Q<sub>0</sub> = 197 800 (calculated with HFSS) F = 2.9985 GHz  $\beta$  = 6



Cavity body assembly Turning: Half-cell and main-ring



BOC fabrication procedure







EBW: Half-cell to virole



Waveguide: T-section











#### First BOC measurements and Blank hole #40



The blank hole #40 was machined, keeping the same diameter as others. The hole depth was optimised to minimize reflection, Finally -21 dB reflection after 6  $\mu$ sec was achieved.









# BOC detuning and HOM damping







Final assembly







# 3 GHz RF Pulse Compressors Gallery



LIPS (XX century)



BOC (XXI century)





Future plans ...





The linear part of the phase slop will be



Flat top compressed pulse with special RF phase modulation

#### Simulations:



Cavity:  $Q_0 = 1.8 \times 10^5$ ,  $\beta = 6$ 





System operation stability issues.

Because of the energy spread, the demand on the compressed pulse flatness is:  $\underline{\Delta P/P < 2\%}$ 

The main sources of instability:

1 Klystron RF phase and amplitude jitter as result of HV supply instability.



The examples of the compressed RF pulse distortion due to the klystron RF phase ripples.

a) RF Phase modulation. Klystron RF phase ripples 3<sup>o</sup> peak-to-peak.



The klystron RF ripples were successfully compensated with RF phase correction of the drive signal.





2 The frequency deviation of the storage cavity, mainly because of the temperature variation.

3 The identity of the LIPS cavities resonant frequencies.



$$\Delta T_s = \frac{\Delta F}{F\alpha}, \quad \alpha = 1.661 \times 10^{-5} \frac{1}{^{o}C}, \quad \Delta F = 1.5 kHz \qquad \Delta T_s = \pm 0.03 \quad ^{o}C$$

To keep the flatness of the compressed pulse within specified  $\Delta P/P$ , the temperature stabilization of the cavity must be  $\Delta T < \pm 0.03 \ ^{\circ}C$ .





BOC high power tests with RF phase modulation.



Solid line - measurements, broken simulations. Data for simulations (Q-factor, coupling) were taken from BOC cold measurements.